

Specialists in Explosives, Blasting and Vibration **Consulting Engineers** 

# **Blast Impact Analysis Uppers Quarry** Part of Lots 119, 120, 136 and 137, Part of the road allowance between Lots 120 and 136 (Geographic Township of Stamford), City

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Submitted to:

of Niagara Falls, Regional Municipality of Niagara

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# **EXECUTIVE SUMMARY**

Explotech Engineering Ltd. was retained in November 2016 to provide a Blast Impact Analysis for the proposed Uppers Quarry located on Part of Lots 119, 120, 136 and 137. The Assessment also takes into account potential extraction of the portion of Upper's Lane and part of the unopened road allowance between Lots 120 and 136 (geographic township of Stamford), where they exist between Thorold Townline Road and Beechwood Road, all in the City of Niagara Falls, Regional Municipality of Niagara.

Vibration levels assessed in this report are based on the Ministry of the Environment, Conservation and Parks (MECP) Model Municipal Noise Control By-law with regard to guidelines for blasting in Mines and Quarries. We have assessed the area surrounding the proposed licence area as it relates to potential damage from blasting operations and compliance with the aforementioned By-law document.

We have inspected the property and reviewed the available site plans. Explotech is of the opinion that the planned aggregate extraction on the proposed property can be carried out safely and within MECP guidelines as set out in NPC 119 of the By-Law.



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# **INTRODUCTION**

Walker Aggregates (Walker) intends to apply for a Class A, Category 2 Licence for the property legally described as Part of Lots 119, 120, 136 and 137, former Township of Stamford, now in the City of Niagara Falls, in the Regional Municipality of Niagara. Two municipal road allowances (Upper's Lane and an unopened road allowance between Part of Lots 120 and 136 in the former Township of Stamford) separate the proposed quarry site into three extraction areas:

- i) North Extraction Area: extraction area North of Upper's Lane;
- ii) Mid Extraction Area: extraction area South of Upper's Lane and North of the unopened road allowance between Township Lots 120 & 136 in the former Township of Stamford, now in the City of Niagara Falls ("unopened road allowance"); and
- iii) South Extraction Area: extraction area South of the unopened road allowance. Part of the road allowance between Lots 120 and 136 (geographic township of Stamford), City of Niagara Falls, Regional Municipality of Niagara.

This Blast Impact Analysis assesses the ability of the proposed licence (whether the two road allowances are ultimately included in the extraction area or not) to operate within the prescribed blast guideline limits as required by the Ontario Ministry of the Environment, Conservation and Parks (MECP).

While not specifically required as part of the scope of the Blast Impact Analysis under the Aggregate Resources Act, this report also touches on the topics of the flyrock and residential water wells for general informational purposes only. Details related to residential water wells are addressed in the hydrogeological report while specific flyrock control is addressed at the operational level given significant influences related to blast design, geology and field accuracy. Additionally, potential impacts on the adjacent TC Energy pipeline, electrical transmission towers, and nearby waterbodies are discussed to confirm compliance with applicable external corporate policies and guidelines.

The proposed Uppers Quarry operation is bounded by farm land to the North and South, Beechwood Road to the East, a residential subdivision (Fernwood) to the Southeast and Thorold Townline Road to the West. A residential and employment subdivision (Rolling Meadows) has been approved West of Thorold Townline Road. The extraction areas will be accessed via Thorold Townline Road and Upper's Lane.



The proponent currently owns the lands housing the residences designated as 5872 Thorold Townline Road and 5497 Beechwood Road. The closest sensitive receptor not owned by the proponent is the property designated as 5329 Beechwood Road.

This Blast Impact Analysis has been prepared based on the MECP Model Municipal Noise Control By-law with regard to Guidelines for Blasting in Mines and Quarries (NPC 119).

Given that mining operations have not been undertaken in the past on this property, site-specific blast monitoring data is not available. We have therefore applied data generated across a spectrum of quarries and construction projects which provides a conservative approximation of anticipated vibration levels from the operation. It has been our experience that this data represents a conservative starting point for blasting operations. It is a recommendation of this report that a vibration monitoring program be initiated on-site upon the commencement of blasting operations and maintained for the duration of all blasting activities to confirm compliance with MECP guideline limits for ground vibration and overpressure based on actual measurements taken during blast times.



# **EXISTING CONDITIONS**

The licenced area for the proposed Uppers Quarry encompasses a total area of approximately 103.6HA. The total extraction area is approximately 89.1HA.

The site is separated into eight (8) extraction phases. The phases are designated as 1a, 1b, 2a, 2b, 3a, 3b, 4 and 5 with phased extraction progressing initially from the Northwest corner of Phase 1a along the West end of the property (Refer to Appendix A).

The topography of the proposed licence area is generally lowest in the North portion of the site at an elevation in the order of 177masl rising towards the West and South with the highest elevations (185masl) lying in the middle of the West boundary of the site (Phase 1b). The design final quarry floor elevation is 141masl –148.7masl leading to the likely execution of 2 to 3 benches to achieve final grade.

The lands surrounding the proposed licence area are largely characterized by agricultural areas with a limited number of residential structures within 500m aside from a subdivision located Southeast of the boundary limits. All sensitive receptors within 500m of the licence boundary are as follows:

Address	Distance to Receptor from Licence Boundary (m)	Direction from Licence Boundary
9337 Beaversdam Road	475	North
9417 Beaversdam Road	447	North
9582 Beaversdam Road	151	North
9722 Beaversdam Road	234	North
10138 Beaversdam Road	442	North
10148 Beaversdam Road	184	North
5329 Beechwood Road	63	East
5584 Beechwood Road	81	Southeast
5769 Beechwood Road	287	Southeast
5821 Beechwood Road	360	Southeast
9312 Madison Crescent	417	Southeast
9315 Madison Crescent	445	Southeast
9324 Madison Crescent	404	Southeast
9325 Madison Crescent	434	Southeast



	Distance to Receptor	Direction from
Address	from Licence Boundary	Licence
71441000	(m)	Boundary
9336 Madison Crescent	390	Southeast
9337 Madison Crescent	423	Southeast
9349 Madison Crescent	415	Southeast
9352 Madison Crescent	370	Southeast
9361 Madison Crescent	407	Southeast
9366 Madison Crescent	354	Southeast
9373 Madison Crescent	391	Southeast
9380 Madison Crescent	338	Southeast
9385 Madison Crescent	371	Southeast
9397 Madison Crescent	351	Southeast
9409 Madison Crescent	334	Southeast
9421 Madison Crescent	316	Southeast
9433 Madison Crescent	299	Southeast
9445 Madison Crescent	280	Southeast
9457 Madison Crescent	260	Southeast
5599 Osprey Avenue	251	Southeast
5607 Osprey Avenue	259	Southeast
5610 Osprey Avenue	311	Southeast
5615 Osprey Avenue	271	Southeast
5622 Osprey Avenue	323	Southeast
5623 Osprey Avenue	284	Southeast
5631 Osprey Avenue	290	Southeast
5632 Osprey Avenue	331	Southeast
5639 Osprey Avenue	299	Southeast
5642 Osprey Avenue	341	Southeast
5647 Osprey Avenue	311	Southeast
5652 Osprey Avenue	350	Southeast
5655 Osprey Avenue	321	Southeast
5663 Osprey Avenue	333	Southeast
5668 Osprey Avenue	362	Southeast
5671 Osprey Avenue	339	Southeast
5679 Osprey Avenue	350	Southeast
5687 Osprey Avenue	362	Southeast
5695 Osprey Avenue	374	Southeast

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	Distance to Receptor	Direction from
Address	from Licence Boundary	Licence
7 (3.3)	(m)	Boundary
5703 Osprey Avenue	383	Southeast
5711 Osprey Avenue	393	Southeast
5719 Osprey Avenue	404	Southeast
5727 Osprey Avenue	415	Southeast
5735 Osprey Avenue	424	Southeast
5743 Osprey Avenue	438	Southeast
5751 Osprey Avenue	448	Southeast
5759 Osprey Avenue	459	Southeast
5767 Osprey Avenue	470	Southeast
5772 Osprey Avenue	499	Southeast
5775 Osprey Avenue	480	Southeast
5783 Osprey Avenue	490	Southeast
9245 Shoveller Drive*	410	Southeast
9314 Shoveller Drive	494	Southeast
9324 Shoveller Drive	488	Southeast
9334 Shoveller Drive	478	Southeast
9344 Shoveller Drive	467	Southeast
9354 Shoveller Drive	460	Southeast
9364 Shoveller Drive	450	Southeast
9374 Shoveller Drive	443	Southeast
9385 Shoveller Drive	392	Southeast
9394 Shoveller Drive	428	Southeast
9395 Shoveller Drive	383	Southeast
9404 Shoveller Drive	423	Southeast
9405 Shoveller Drive	374	Southeast
9414 Shoveller Drive	416	Southeast
9424 Shoveller Drive	412	Southeast
9434 Shoveller Drive	405	Southeast
9446 Shoveller Drive	400	Southeast
9045 Eagle Ridge Drive	457	Southeast
9355 Eagle Ridge Drive	494	Southeast
9365 Eagle Ridge Drive	481	Southeast
9375 Eagle Ridge Drive	469	Southeast
9385 Eagle Ridge Drive	471	Southeast



Address	Distance to Receptor from Licence Boundary (m)	Direction from Licence Boundary
9395 Eagle Ridge Drive	464	Southeast
9415 Eagle Ridge Drive	448	Southeast
9425 Eagle Ridge Drive	445	Southeast
9435 Eagle Ridge Drive	443	Southeast
9440 Eagle Ridge Drive*	484	Southeast
9445 Eagle Ridge Drive	436	Southeast
9461 Eagle Ridge Drive	427	Southeast
9484 Eagle Ridge Drive	480	Southeast
9490 Eagle Ridge Drive	478	Southeast
9494 Eagle Ridge Drive	477	Southeast
9500 Eagle Ridge Drive	474	Southeast

<sup>\*</sup>Multiple units located at address, closest unit to licence boundary included above

# Table 1: Sensitive Receptors within 500m of the Licence Boundary

The properties on the proposed licenced land (5205 and 5497 Beechwood Road, 5872 Thorold Townline Road, 9764 Upper's Lane, 9903 Upper's Lane and 10200 Upper's Lane) are within the proposed extraction limits. Upon commencement of extraction, the use of these structures will be such that they do not qualify as sensitive receptors.

The utility buildings (4832 Thorold Townline Road) located directly adjacent the proposed licence do not qualify as sensitive receptors as defined by the MECP (refer to Appendix E for Definitions) but will remain in place and operational for the foreseeable future. In order to safeguard the integrity of this structure, we recommend that vibrations at the utility buildings be maintained below 50mm/s in accordance with research performed by the United States Bureau of Mines (USBM RI8507). It is a recommendation of this report that this structure shall be monitored for ground vibration when vibration calculations suggest vibrations in excess of 35mm/s.



# PROPOSED MINERAL EXTRACTION

An existing watercourse runs North-South through Phase 3a, Phase 4 and Phase 5 of the extraction limits. The proposed existing watercourse realignment will relocate the watercourse inside the excavation limits on the Western limits of extraction inside Phase 1b and 2b.

The extraction operations will begin with a sinking cut at the Northwest portion of Phase 1a (Mid Extraction Area) and will retreat Easterly and Southerly through Phase 1a. Phase 1b is located on the Western edge of Phase 1a and borders the Western most boundary for the proposed licence. In the Mid Extraction Area, Phase 1a will be extracted to a final floor elevation of 141 – 145masl and given existing topography of 181 – 185masl, it is anticipated that Phase 1a extraction will take place in 2 – 3 benches. Phase 1b will be extracted to a depth of no greater than 155masl in order to facilitate the construction of the new realigned watercourse. The Phase 1a and Phase 1b areas are also located in the South Extraction area separated by a road allowance not owned by the proponent. As a result, an additional sinking cut in the Northwest corner of Phase 1a (South Extraction Area) will be required. Phase 1a (South Extraction Area) will retreat Easterly and Southerly through Phase 1a (South Extraction Area). Phase 1b (South Extraction Area) is located on the Western edge of Phase 1a and borders the Western most boundary for the proposed licence. In the South Extraction Area, Phase 1a will be extracted to a final floor elevation of 141 – 145 masl and given existing topography of 182 – 185masl, it is anticipated that Phase 1a (South Extraction Area) extraction will take place in 2 – 3 benches. Phase 1b (South Extraction Area) will be extracted to a depth of no greater than 155masl in order to facilitate the construction of the new realigned watercourse.

Phase 2a (North Extraction Area) is located North of Phase 1a and will begin with a sinking cut at the Southwest corner of Phase 2a and will retreat Easterly and Northerly through Phase 2a. Phase 2b is located on the Western and Northern edge of Phase 2a and borders the Western most boundary for the proposed licence. Phase 2a will be extracted to a final floor elevation of 144 – 145masl and given existing topography of 180 – 182masl, it is anticipated that Phase 2a extraction will take place in 2 – 3 benches. Phase 2b will be extracted to a depth no greater than an elevation of 155masl in order to facilitate the construction of the new realigned watercourse whereas the watercourse alignment transition area found at the North end of Phase 2b will only be extracted to a depth of no greater than 174masl in order to facilitate the construction of the new realigned watercourse.

Phase 3a (North Extraction Area) is located to the East of Phase 2a and is currently traversed by the existing watercourse. The existing watercourse is to be



relocated to the West perimeter of the site after the successful completion of the Phase 1b and 2b extraction.

A sinking cut in the Southwest corner of Phase 3b will initiate extraction with a Northerly and Easterly retreat. Extraction for Phase 3a will leverage the face created by extraction in Phase 2a with a Easterly retreat. \*\*\*

Phase 3a/3b will be extracted to a final floor elevation of 146masl – 149masl and given existing topography of 177masl – 183masl, it is anticipated that Phase 3 extraction will take place in 2 – 3 benches.

Phase 4 is located in the middle of the proposed licence area (Mid Extraction Area) and progresses from the Eastern Phase 1a limit (Mid Extraction Area) Easterly to the East proposed extraction limits. Extraction of Phase 4 will utilize the Eastern face of Phase 1a and will be extracted in 2 – 3 benches to a depth ranging from 141masl – 149masl given existing topography in Phase 4 of 177masl - 184masl.

Phase 5 is located in the South of the proposed licence area (South Extraction Area) and progresses from the Eastern Phase 1a limit (South Extraction Area) Easterly to the South and East extraction limits. Extraction of Phase 5 will utilize the Eastern face of Phase 1a and will be extracted in 2 – 3 benches to a depth ranging from 141masl – 149masl given existing topography in Phase 5 of 178masl - 182masl.

All extraction phases bordering the perimeter limits of the quarry (namely phases 1b, 2b, and 3a) will have a catchment bench located at elevation 149masl – 155masl depending on the phase.

As quarry operations migrate across the property, the closest sensitive receptors to the required blasting operations will vary. The closest receptor to the proposed Upper's Quarry licence area over the life of the quarry is 5329 Beechwood Road at a distance of 63m from the licence boundary.

\*\*\*Alternatively, if the existing watercourse is realigned prior to the extraction operations in Phase 3, extraction may begin in Phase 3a. Phase 3a will leverage the existing Phase 2a face and retreat Easterly. Phase 3b will then leverage the Phase 3a face and retreat Easterly. If this alternate extraction proceeds, the conclusions of this report are unchanged.



# BLAST VIBRATION AND OVERPRESSURE LIMITS

The Ontario MECP guidelines for blasting in quarries are among the most stringent in North America.

Studies by the U.S. Bureau of Mines have shown that normal temperature and humidity changes can cause more damage to residences than blast vibrations and overpressure in the range permitted by the MECP. The guideline limits set by the MECP are as follows.

Vibration	12.5mm/sec	Peak Vector Sum (PVS)
Overpressure	128 dBL	Peak Sound Pressure Level (PSPL)

The above guidelines apply when blasts are being monitored. Cautionary levels are slightly lower and apply when blasts are not monitored on a routine basis. It is a recommendation of this report that all blasts at the operation be monitored to quantify and record ground vibration and overpressure levels employing a minimum of two (2) digital seismographs, one installed at the closest sensitive receptor in front of the blast, or closer, and a second installed at the closest sensitive receptor behind the blast, or closer.



# **BLAST MECHANICS AND DERIVATIVES**

The detonation of explosives within a borehole results in the development of very high gas and shock pressures. This energy is transmitted to the surrounding rock mass, crushing the rock immediately surrounding the borehole (approximately 1 borehole radius) and permanently distorts the rock to several borehole diameters (5-25, depending on the rock type, prevalence of joint sets, etc.).

The intensity of this stress wave decays quickly so that there is no further permanent deformation of the rock mass. The remaining energy from the detonation travels through the unbroken material in the form of a pressure wave or shock front which, although it causes no plastic deformation of the rock mass, is transmitted in the form of vibrations.

Particle velocity is the descriptor of choice when dealing with vibrations because of its superior correlation with the appearance of cosmetic cracking. As such, for the purposes this report, ground vibration units have been listed in mm/s.

In addition to the ground vibrations; overpressure, or air vibrations are generated through the direct action of the explosive venting through cracks in the rock or through the indirect action of the rock movement. In either case, the result is a pressure wave which travels through the air, measured in decibels (or dB) for the purposes of this report.



# **VIBRATION AND OVERPRESSURE THEORY**

Transmission and decay of vibrations and overpressure can be estimated by the development of attenuation relations. These relations utilize empirical data relating measured velocities at specific separation distances from the vibration source to predict particle velocities at variable distances from the source. While the resultant prediction equations are reliable, divergence of data occurs as a result of a wide variety of variables, most notably site-specific geological conditions and blast geometry and design for ground vibrations and local prevailing climatic conditions for overpressure.

In order to circumvent this scatter and improve confidence in forecast vibration levels, probabilistic and statistical modeling is employed to increase conservatism built into prediction models, usually by the application of 95% confidence lines to attenuation data.

The attenuation relations are not designed to conclusively predict vibration levels at a specific location as a result of a specific blast design, application of this probabilistic model creates confidence that for any given scaled distance, 95% of the resultant velocities will fall below the calculated 95% regression line.

While the data still provides insight into probable vibration intensities, attenuation relations for overpressure tends to be less reliable and precise than results for ground vibrations. This is due primarily to wider variations in variables outside of the influence of the blast design which impact propagation of the vibrations. Atmospheric factors such as temperature gradients and prevailing winds (refer to Appendix B) as well as local topography can all serve to significantly alter overpressure attenuation characteristics. Fortunately, as described above, the conservatism built into the equations and the on-site vibration and overpressure monitoring performed at the quarry will aid in quantifying the vibrations and overpressures specific to the area in order to further reduce the likelihood of damage to all structures adjacent the quarry limits.

Our experience and analysis demonstrates that blast overpressure is greatest when blasting towards receptors, and blast vibrations are greatest when retreating towards the receptors.



# **GROUND VIBRATION LEVELS AT THE NEAREST SENSITIVE RECEPTOR**

The most commonly used formula for predicting Peak Particle Velocity (PPV) is known as the Bureau of Mines (BOM) prediction formula or Propagation Law. We have used this formula to predict the PPV's at the closest house for the initial operations.

$$PPV = k \left(\frac{d}{\sqrt{w}}\right)^e$$

Where, PPV = the predicted peak particle velocity (mm/s)

K, e = site factors

d = distance from receptor (m)

w = maximum explosive charge per delay (kg)

The value of K and e are variable and influenced by many factors (i.e. rock type, geology, thickness of overburden, etc.). As such, these site factors are developed empirically through the measurement of vibration characteristics at the specific operations of interested.

The portion of the BOM prediction formula contained within the parentheses is referred to as the *Scaled Distance* and represents another important PPV relation. It correlates the separation distance between a blast and receptor to the energy (usually expressed as explosive weight) released at any given instant in time. The two most popular approaches are square root scaling and cube root scaling:

$$(SDSR = \frac{R}{\sqrt{W}})$$
  $(SDCR = \frac{R}{\sqrt[3]{W}})$ 

Where, SDSR = Scaled distance square root method

SDCR = Scaled distance cube root method

R = Separation distance between receptor site and blast (m)

W = Maximum explosive load per delay period (kg)

Historically, square root scaling is employed in situations whereby the explosive load is distributed in a long column (i.e. blasthole) while cube root scaling is employed for point charges. In accordance with industry standard, square root scaling was adopted for ground vibration analysis for the purposes of this report.



For a distance of 710m (the standoff distance to the closest sensitive receptor for the initial Phase 1a blasting (Mid Extraction Area), namely 10148 Beaversdam Road) and a maximum explosive load per delay of 118kg (101mm diameter hole, 15m deep, 3m surface collar and 1 hole per delay), we can calculate the maximum PPV at the closest building using the following formulae:

# Imperial Equations:

Oriard 50% Bound (2002)	$v = 160(\frac{D}{\sqrt{W}})^{-1.6}$
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Oriard 90% Bound (2002) 
$$v = 242(\frac{D}{\sqrt{W}})^{-1.6}$$

Quarry Production Blast (Bulletin 656 – 1971) 
$$v = 182(\frac{D}{\sqrt{W}})^{-1.82}$$

Typical limestone Quarry (Pader report – 1995) 
$$v = 52.2(\frac{D}{\sqrt{W}})^{-1.38}$$

Typical Coal Mine 
$$v = 133(\frac{D}{\sqrt{W}})^{-1.5}$$
 (RI8507 1980)

# Metric Equations:

General Blasting 
$$v = 1140(\frac{D}{\sqrt{W}})^{-1.6}$$
 (Dupont)

Construction Blasting (Dowding 1998) 
$$v = 1326(\frac{D}{\sqrt{W}})^{-1.38}$$

Agg. Quarry Blasting (Explotech 2005) 
$$v = 5175 \left(\frac{D}{\sqrt{W}}\right)^{-1.76}$$

Agg. Quarry blasting (Explotech 2003) 
$$v = 7025 (\frac{D}{\sqrt{W}})^{-1.85}$$



The equations described above accommodate for a range of geological conditions. The proposed blast parameters were applied to the formulae to estimate a range of the potential vibrations to be imparted on the closest sensitive receptor behind the blast. As discussed in previous sections, the MECP guideline for blast-induced vibration is 12.5 mm/s (0.5 in/s). Appendix C demonstrates that the maximum (ie worst-case) calculated value for the vibration intensities imparted on the closest sensitive receptor based on all equations is 4.14mm/s for the initial blasting, well below the MECP guideline limit. All blasts will be monitored for overpressure and ground vibrations with blast designs adjusted in response to readings on site in order to confirm consistent compliance with established limits.

All vibration calculations and tables going forward will utilize the formula providing the worst case scenario for all geological conditions (Construction Blasting (Dowding 1998)).

An **example** of this calculation is as follows:

For a distance of 710m (the standoff distance to the closest sensitive receptor for the initial Phase 1a blasting, namely 10148 Beaversdam Road) and a maximum explosive load per delay of 118kg (101mm diameter hole, 15m deep, 3m surface collar and 1 hole per delay), we can calculate the maximum PPV at the closest sensitive receptor as follows:

$$ppv = 1326 \left(\frac{710}{\sqrt{118}}\right)^{-1.38} = 4.14 mm/s$$

As discussed in previous sections, the MECP guideline for blast-induced vibration is 12.5 mm/s (0.5 in/s). The calculated 95% predicted PPV (based on the proposed blasting data discussed above) would be 4.14mm/s, well below the MECP guideline limit. It is understood that as separation distance to the receptors decreases, adjustments to blast designs may be necessary to maintain compliance with the guideline limits.

Similarly, the above equation used to calculate PPV can be reformatted to find an approximation of the distance at which a vibration velocity of 12.5mm/s would occur if all blasting parameters are kept the same as used in the equation above:

$$12.5 = 1326 \left(\frac{d}{\sqrt{118}}\right)^{-1.38} = 319.0m$$



The above result suggests that design modifications to the above preliminary design of an explosive load of 118kg/delay would be required once blasting operations encroach to within 319m of any sensitive receptor. Fortunately, vibration data will be continually collected and analyzed as the sensitive receptors are approached in order to confirm the requirement for any design modifications. An abundance of design modifications are available which would readily maintain vibration intensities below guideline limits. This is based on conservative assumptions which will be confirmed through monitoring.

Given the separation distances that will be involved at the proposed Uppers Quarry, Table 2 below provides initial guidance on maximum loads per delay based on various separation distances. The following maximum loads per delay were derived from the equation for ground vibrations listed above and are based on a maximum intensity of 12.5mm/s:

Separation distance between sensitive receptor and closest borehole (meters)	Maximum recommended explosive load per delay (Kilograms)
500	290
450	235
400	185
350	140
300	105
250	70
200	45
150	25
100	11

Table 2: Maximum Loads per Delay to Maintain 12.5mm/s at Various Separation Distances

It is noteworthy that the above values are typically conservative and are intended as a guideline only as the ground vibration attenuation equation is based on a calculated 95% regression line. Actual loads can be adjusted on the basis of the results of the monitoring program in place.

The closest separation distance between a sensitive receptor and the licence boundary is 63m. While blasting at this separation distance is feasible from a technological perspective, given current blasting technology and techniques, market economics will dictate the feasibility of extracting rock at lesser separation distances. Monitoring and changes in blasting designs will be required in order to



confirm all blasts are within MECP guidelines when blasting comes closer to adjacent sensitive receptors.

Similarly to the paragraph above, the closest separation distance between a <u>non-sensitive receptor</u> (namely the utility buildings located at 4832 Thorold Townline Road) and the extraction limits of the licence is 40m. Using the above equation and keeping the same blasting parameters with a suggested limit of 50mm/s, the calculation would suggest that once blasting encroaches to 116m removed from the utility buildings, modifications may be required.



# OVERPRESSURE LEVELS AT THE NEAREST SENSITIVE RECEPTOR

It is unusual for overpressure to reach damaging levels and when it does, the evidence is typically immediate and obvious in the form of broken windows in the area. However, overpressure remains of interest due to its ability to travel further distances as well as cause audible sounds and excitation in windows and walls.

Air overpressure decays in a known manner in a uniform atmosphere, however, a uniform atmosphere is not a normal condition. As such, air overpressure attenuation is far more variable due to its intimate relationship with environmental influences. Air vibrations decay slower than ground vibrations with an average decay rate of 6dBL for every doubling of distance.

Air overpressure levels are analyzed using cube root scaling based on the following equation:

$$P = k \left(\frac{d}{\sqrt[3]{w}}\right)^e$$

Where, P = the peak overpressure level (psi – imperial, Pa, dB - metric)

K, e = site factors

d = distance from receptor (ft – imperial, m - metric)

w = maximum explosive charge per delay (lbs – imperial, kg - metric)

The value of K and e are variable and are influenced by many factors (i.e. rock type, geology, thickness of overburden, environmental conditions, etc.). As such, these site factors are developed empirically through the measurement of overpressure characteristics at the specific operations of interested.

As discussed in previous sections, the MECP guideline for blast-induced overpressure is 128dBL. For a distance of 710m (i.e. the standoff distance to the closest sensitive receptor in front of the blast for the initial Phase 1a blasting (Mid Extraction Area), namely 10148 Beaversdam Road) and a maximum explosive load of 118kg (101mm diameter hole, 15m deep, 3m surface collar and 1 hole per delay), we can calculate the overpressure at the nearest receptor in front of the blast using the following equations:

# EXPLOTECH

# Imperial Equations:

USBM RI8485 (Behind Blast) 
$$P = 0.056 (\frac{D}{\sqrt[3]{W}})^{-0.515}$$

USBM RI8485 (Front of Blast) 
$$P = 1.317 (\frac{D}{\sqrt[3]{W}})^{-0.966}$$

USBM RI8485 (Full Confined) 
$$P = 0.061 (\frac{D}{\sqrt[3]{W}})^{-0.96}$$

Construction Average (Oriard 2005) 
$$P = 1(\frac{D}{\sqrt[3]{W}})^{-1.1}$$

# Metric Equations:

Ontario Quarry - dB 
$$P = 159(\frac{D}{\sqrt[3]{W}})^{-0.0456}$$
 (Explotech)

Limestone - dB 
$$P = 206 (\frac{D}{\sqrt[3]{W}})^{-0.1}$$
 (Explotech)

Ontario Quarry - Pa 
$$P = 1222 \left(\frac{D}{\sqrt[3]{W}}\right)^{-0.669}$$
 (Explotech)

Appendix C demonstrates that the maximum calculated value for the overpressure intensities imparted on the closest sensitive receptor based on all equations is 126.8 dB(L) for the initial blasting, below the MECP guideline limit. For initial blasting, all blasts should be scheduled on days with favourable weather conditions to assist in mitigating overpressure levels.

The initial blasting area is also located in the most optimal location such that the direction of extraction will only increase the distance removed from where the front face is directed towards the sensitive receptor. Every subsequent blast in Phase 1a when retreating to the East and South from the initial Phase 1a sinking cut area will result in progressively lower overpressure results. All blasts will be monitored for overpressure and ground vibrations with blast designs adjusted in response to readings on site in order to maintain consistent compliance with established limits.



Based on the above calculation and the assumed blast parameters, and the conservatism built into the equations, overpressures from blasting operations can remain compliant with the MECP NPC 119 guideline limit of 128dBL. The design method of retreat has been planned so as to direct overpressures generated as much as practicable in the direction of vacant lands. All overpressure calculations and tables going forward will utilize the formula providing the worst case scenario for all geological conditions (Ontario Quarry – Pa (Explotech)).

We reiterate that air overpressure attenuation is far more variable due to its intimate relationship with environmental influences and as such, the equation employed is less reliable than that developed for ground vibration. Overpressure monitoring performed on site shall be used to guide blast design as it pertains to the control of blast overpressures. As demonstrated in Appendix B, prevailing winds during quarry operational periods are predominantly out of the Southwest.

The overpressure equation used to calculate PSPL can be reformatted to find an approximation of the distance at which an overpressure of 128 dB(L) would occur. If all blasting parameters are kept the same as above, a distance of 580m from the closest sensitive receptor in front of the blast would have a calculated overpressure of 128db(L). Once again, the on-site monitoring program will accurately delineate the overpressure intensities and provide guidance for the timing for any design changes.

Given the correlation between overpressure and environmental conditions as stated previously, care must be taken to avoid blasting on days when weather patterns are less favourable. Extraction directions have been selected so as to minimize overpressure impacts on adjacent receptors.

Table 3 below can be used as an initial guide showing maximum loads per delay based on various separation distances for receptors in front of the blast face. The following maximum loads per delay are derived from the air overpressure equation above and are based on a peak overpressure level of 128dB(L):



Separation distance between sensitive receptor and closest blasthole (meters)	Maximum recommended explosive load per delay (Kilograms)
1000	610
900	440
800	310
700	208
600	130
500	75

Table 3: Maximum Calculated Loads per Delay to Maintain 128dB(L) at Various Separation Distances for Receptors in Front of the Face

We note that the above values are conservative and are intended as a guideline only as the air overpressure attenuation is based on a calculated 95% regression line. Actual loads employed shall be based on the results of the monitoring program in place.



# ADDITIONAL CONSIDERATIONS OUTSIDE OF THE BLAST IMPACT ANALYSIS SCOPE

The following headings are addressed for general information purposes and are not strictly required as part of the scope of the Blast Impact Analysis as required under the ARA to assess compliance with MECP NPC-119 guidelines. Considerations for the TC Energy Pipeline and Hydro One transmission towers can be expanded upon under separate cover with direct input from the owners as required. The hydrogeological study prepared by WSP as part of the licence application will address residential water wells in detail. Flyrock control is addressed at the operational level given significant influences related to blast design, geology and field accuracy which render concrete recommendations related to control inappropriate at the licencing phase. Considerations for aquatic species in the existing watercourse are further addressed in the Stantec report.

# TC ENERGY HIGH PRESSURE NATURAL GAS PIPELINE

A TC Energy High Pressure Natural Gas Pipeline runs adjacent to the Northwest corner of the proposed quarry limits (refer to Appendix A). The MECP guideline for blast-induced vibration (12.5mm/s) does not apply to pipelines as they are not classified as sensitive receptors. Two (2) welded steel pipelines exist within the TC Energy right of way (ROW), one 20" and one 36" diameter pipeline. TC Energy Policy employs a 50mm/s vibration limit for welded steel pipelines. Based on the proposed Operations Plan for the Uppers Quarry, initial blasting operations are anticipated to be required approximately 345m from the subject pipeline, however, will reach as close as 7m throughout the course of extraction.

Applying the equation from Predicated Vibration Limits at the Nearest Sensitive Receptor, for a distance of 345m (the conservative standoff distance to the pipeline for the initial blasting (Mid Extraction Area)) and a maximum explosives load per delay of 118kg (101mm diameter hole, 15m deep, 3m surface collar and 1 hole per delay), we can calculate the maximum PPV at the pipeline as follows for the initial blast:

$$ppv = 1326 \left( \frac{345}{\sqrt{118}} \right)^{-1.38} = 11.22 mm/s$$

The calculated 95% predicted PPV (based on the proposed blasting data discussed above) would be 11.22mm/s, well below the TC Energy limit of 50mm/s for a steel welded pipeline located adjacent to the proposed quarry.



While this initial value resides below the required threshold, it is anticipated that design modifications will be necessary to maintain compliance as the separation distance to the pipeline decreases and column loads increase. Fortunately, a variety of blast design alternatives are available to accomplish this including but not limited to reductions in blast hole diameter, change in explosives types, adjustment in bench heights and decking of holes.

We do note that the TC Energy Blasting Specification requires the presence of a vibration monitoring program when blasting operations are to be conducted within 100m of a pipeline. The proposed Operational Plan dictates that blasting is to encroach within 7m of the ROW and as such, it is a recommendation of this report that an independent third party firm be retained to conduct vibration monitoring on this pipeline when separation encroaches within 100m of the pipeline or when calculations suggest ground vibrations in excess of 35mm/s as measured at the pipeline are anticipated. The results of this monitoring program will determine what blast design alterations shall be necessary as the separation distance to the subject pipeline decreases. Walker will adhere to the guidelines set by TC Energy with respect to blasting in proximity of the gas lines.



#### FLYROCK

Flyrock is the term used to define rocks which are propelled from the blast area by the force of the explosion. This action is a predictable and necessary component of a blast and requires that every blast have an exclusion zone established within which no persons or property which may be harmed are permitted.

Government regulations strictly prohibit the ejection of flyrock off of a quarry property. The regulations regarding flyrock are enforced by the Ministries of Natural Resources, Environment and Labour. In the event of an incident where flyrock does leave a site, the punitive measures include suspension / revocation of licences and fines to both the blaster and quarry owner / operator. Fortunately, flyrock incidents are extremely rare due to the possible serious consequences of such an event. It is in the best interest of all, stakeholders and non-stakeholders, to ensure that dangerous flyrock does not occur. Through proper blast planning and design, it is possible to control and mitigate the possibility for flyrock.

# THEORETICAL HORIZONTAL FLYROCK CALCULATIONS

Flyrock occurs when explosives in a hole are poorly confined by the stemming or rock mass and the high pressure gas breaks out of confinement and launches rock fragments into the air. The three primary sources of fly rock are as follows:

- **Face burst:** Lack of confinement by the rock mass in front of the blast hole results in fly rock in front of the face.
- Cratering: Insufficient stemming height or weakened collar rock results in a crater being formed around the hole collar with rock projected in any direction.
- **Stemming Ejection:** Poor stemming practice can result in a high angle throw of the stemming material and loose rocks in the blasthole wall and collar

The horizontal distance flyrock can be thrown ( $L_H$ ) from a blast hole is determined using the expression:

$$L_{H} = \frac{V_{o}^{2} Sin2\theta_{0}}{g}$$
 [1]



where:  $V_o = \text{launch velocity (m/s)}$ 

 $\theta_0$  = launch angle (degrees)

 $g = \text{gravitational constant } (9.8 \text{ m/s}^2)$ 

The theoretical maximum horizontal distance fly rock will travel occurs when  $\theta_0$  = 45 degrees, thereby yielding the equation:

$$L_{H \max} = \frac{V_o^2}{g}$$
 [2]

The normal range of launch velocity for blasting is between 10m/s - 30m/s. To calculate the launch velocity of a blast the following formula is used:

$$V_o = k \left(\frac{\sqrt{m}}{B}\right)^{1.3}$$
 [3]

where: k = a constant

m = charge mass per meter (kg/m)

B = burden (m)

By combining equations 2 and 3 and taking into account the different sources of fly rock, the following equations can be used to calculate the maximum fly rock thrown from a blast:

Face burst: 
$$L_{H \max} = \frac{k^2}{g} * \left(\frac{\sqrt{m}}{B}\right)^{2.6}$$

Cratering: 
$$L_{H \max} = \frac{k^2}{g} * \left(\frac{\sqrt{m}}{SH}\right)^{2.6}$$



Stemming Ejection: 
$$L_{H \max} = \frac{k^2}{g} * \left(\frac{\sqrt{m}}{SH}\right)^{2.6} Sin2\theta$$

where:  $\theta = \text{drill hole angle}$ 

L<sub>hmax</sub> = maximum flyrock throw (m) m = charge mass per meter (kg/m)

B = burden (m)

SH = stemming height (m) g = gravitational constant

k = a constant

The range for the constant k is 13.5 for soft rocks and 27 for hard rocks. Given the proposed licence area is predominantly limestone, we have applied a k value of 21. The explosive density is assigned to be 1.2 g/cc for emulsion products and the drill hole angles are assumed to be 90 degrees (i.e. vertical).

For calculation purposes, we have applied the initial blasting parameters which utilize 101mm (4") diameter holes on a 3.05m x 3.05m (10' x 10') pattern, with a lift height of 15m (49') and a collar length of 3.0m (10'). The following does not apply to the sinking cut which will require highly specialized designs and additional considerations for flyrock. Based on a free face blast, maximum anticipated horizontal flyrock projection distances are calculated as follows in Table 4:

Table 4 – Maximum Flyrock Horizontal		
<i>Collar</i> Lengths	Maximum Throw Face Burst	Maximum Throw Cratering and Stemming Ejection
(m)	(m)	(m)
1.5	48	302
2.0	48	143
2.5	48	80
3.0	48	50
3.5	48	33



Different collar lengths are displayed in the table above to account for over or under loaded holes. As demonstrated with these various collar lengths, any deviation, no matter how slight, can greatly affect these maximum values. The current proposed initial blasting parameters have the potential to send flyrock 50m assuming all holes achieve the designed collar lengths of 3.0m. Blast mats or sand can be placed on top of the initial blast to further reduce the distance for potential flyrock.

Through proper blast design and diligence in inspecting the geology before every blast, flyrock can readily be maintained within the quarry limits. It may be necessary to increase collars and adjust designs accordingly when blasting along the perimeter to accommodate the reduced deportation distance to receptors and to maintain flyrock within the property limits. The operational plan for the quarry has been designed to retreat towards the closest receptors thereby projecting flyrock and overpressures away from the receptors.



# TRANSMISSION AND HYDRO TOWERS

Transmission towers (Namely the Hydro One Corridor) runs parallel to the Southern limits of the proposed quarry licence noted on the proposed Operational Plan (refer to Appendix A). The MECP guideline for blast-induced vibration (12.5mm/s) does not apply to transmission/hydro towers as they are not classified as sensitive receptors. In order to safeguard the integrity of these structures, Hydro One has set a vibration limit of 50mm/s at the foundations of the transmission towers.

As per direction from Hydro One, calculations will be based on the 50mm/s limit. The tower shall be monitored for ground vibration and overpressure when vibration calculations suggest vibrations in excess of 35mm/s at the tower base. Based on the proposed Operations Plan for the Uppers Quarry, initial blasting operations are anticipated to be approximately 530m from the closest tower, however, will reach as close as 30m throughout the course of extraction at the Southern limits of Phase 1b and Phase 5.

Applying the equation from Predicated Vibration Limits at the Nearest Sensitive Receptor, for a distance of 530m (the conservative standoff distance to the transmission tower for the initial blasting) and a maximum explosives load per delay of 118kg (101mm diameter hole, 15m deep, 3m surface collar and 1 hole per delay), we can calculate the maximum PPV at the transmission tower for the initial blast as follows:

$$ppv = 1326 \left(\frac{530}{\sqrt{118}}\right)^{-1.38} = 6.2 mm/s$$

The calculated 95% predicted PPV (based on the proposed blasting data discussed above) would be 6.2mm/s, well below the limit of 50mm/s. While this value resides below the 50mm/s threshold, it is anticipated that design modifications will be necessary to maintain compliance as the separation distance to some of the towers decreases and column loads increase. Fortunately, a variety of blast design alternatives are available to accomplish this including but not limited to reductions in blast hole diameter, change in explosives types, adjustment in bench heights and decking of holes.



# RESIDENTIAL WATER WELLS

Possible impacts to the water quality and production capacity of groundwater supply wells is a common concern for residents near blasting operations. Complaints related to changes in water quality often include the appearance of turbidity, water discolouration and changes in water characteristics (including nitrate, e-coli, and coliform contamination). Complaints regarding water production most often involve loss of quantity production, air in water and damage to well screens and casings. A review of research and common causes of these problems indicates that most of these concerns are not related to blasting and can be shown to be the direct impact of environmental factors and poor well construction and maintenance.

There is significant research and scientific substantiation demonstrating that outside of the immediate radius of approximately 20-25 blasthole diameters from a loaded hole, there is no permanent ground displacement resulting from a blast. As such, barring blasting activity within several meters of an existing well, the probability of damage to residential wells is essentially non-existent.

Despite the scientific support for the above conclusion, numerous studies have been performed to verify the validity of this statement. These studies have investigated the effects of blasting on varied well configurations and in varied geological mediums to permit conclusions to be readily extrapolated to diverse blasting operations. The conclusion of these studies has confirmed that with the exception of possible temporary increases in turbidity, blasting operations did not result in any permanent impact on wells outside of the immediate blast zone of the blast until vibrations levels reached exceedingly high intensities. Applying universally accepted threshold levels for ground vibrations eliminates the possibility for any long term adverse effects on wells in the vicinity of blasting operations.

In a study by Froedge (1983), blast vibration levels of up to 32.3mm/s were recorded at the bottom of a shallow well located at a distance of 60 meters (200 feet) from an open pit blast. There was no report of visible damage to the well nor was there any change in the water pumping flow rate. This study concluded that the commonly accepted limit of 50mm/s PPV level is adequate to protect wells from any damage. We reiterate, the current guideline limit for vibrations from quarry and mining operations is 12.5mm/s.



Rose et al. (1991) studied the effect of blasting in close proximity to water wells near an open pit mine in Nevada, USA. Blasts of up to 70 kilograms of explosives per delay period were detonated at a distance of 75 meters (245 feet) from a deep water well. There was no reported visible damage to the well. Fluctuations in water level and flow rate were evident immediately after the blast. However, the well water level and flow rate quickly stabilized.

The U.S. Bureau of Mines conducted a study (Robertson et al., 1990) to determine the changes in well capacity and water quality. This involved pumping from wells before and after nearby blasting. One experiment with a well in sandstone showed no change in well capacity after blasts induced PPV's at the surface of 84mm/s and there was no change in water level after PPV's of 141mm/s, well above the current guideline limit of 12.5mm/s.

Matheson et al. (1997) brought together available information on the most common complaints, the possible causes of the complaints and the relation between blasting and the complaint causes. This study yet again reaffirmed the fact that the attribution of well problems to blast sources are unfounded.

The MECP vibration limit of 12.5mm/s effectively excludes any possibility of damage to residential water wells. Based on available research and our extensive experience in Ontario quarry blasting, blasting at the Upper's Quarry will induce no permanent adverse impacts on the residential water wells on properties surrounding the site.



# BLAST IMPACT ON ADJACENT WATERCOURSES

The detonation of explosives in or near water can produce compressive shock waves which initiate damage to the internal organs of fish in close proximity, ultimately resulting in the death of the organism. Additionally, ground vibrations imparted on active spawning beds have the ability to adversely impact the incubating eggs and spawning activity. In an effort to alleviate adverse impacts on fish populations as a result of blasting, the Department of Fisheries and Oceans (DFO) developed the Guidelines for the Use of Explosives In or Near Canadian Fisheries Waters (1998). This publication establishes limits for water overpressure and ground vibrations which are intended to mitigate impacts on aquatic organisms while providing sufficient flexibility for blasting to proceed. Specifically, water overpressures are to be limited to 100kPa and, in the presence of active spawning beds, ground vibrations at the bed are to be limited to 13mm/s.

An existing watercourse currently runs in a North/South direction through the middle of Phase 3a and the Western sections of Phases 4 and 5. The operational plan has proposed for the realignment of the existing watercourse as part of the licence but will remain in its current location during blasting in Phases 1a and 1b. The operational plan shows the existing watercourse alignment, prior to its realignment, at an approximate 26m setback distance from all surrounding phases. Based on these separation distances and our experience on similar operations, water overpressures generated by the blasting will reside below the DFO 100kPa guideline limit and will have no impact on the adult fish populations present.

As per a preliminary document completed by Stantec, one of the fish species identified (Pike) in the adjacent watercourse have two (2) distinct spawning areas but technically anywhere that vegetation is flooded could be potential spawning habitat. The closest area of potential spawning lies approximately 208m from the initial Phase 1a (Mid Extraction Area) Sinking Cut Area blasting operations. The spawning time for the identified fish species in the adjacent watercourses has been established from March – July. As such, active spawning beds present would be subject to the DFO guideline vibration limit of 13mm/s. During spawning season, vibration monitoring will be required at the shoreline adjacent the closest spawning area on the blast side of the water body in order to confirm compliance with DFO limits for ground vibration.



Table 5 below is presented as initial guidance showing maximum permissible loads per delay based on various separation distances from spawning beds. The following maximum loads per delay are derived from the equation for ground vibrations listed earlier in this report and are based on a maximum vibration intensity of 13.0mm/s as experienced at the active spawning habitat:

Separation distance between possible spawning bed and closest borehole (meters)	Maximum recommended explosive load per delay (Kilograms)
500	305
450	245
400	195
350	150
300	110
250	75
200	49
150	27
100	12
75	6.5
50	3
30	1

Table 5: Maximum Loads per Delay to Maintain 13.0mm/s at Various Separation Distances

The generation of suspended solids within the watercourse as a result of the blasting activities will be negligible and grossly subordinate to suspended solids generated as a result of spring runoff and rain activity.



#### RECOMMENDATIONS

It is recommended that the following conditions be applied for all blasting operations at the proposed Upper's Quarry:

- An attenuation study shall be undertaken by an independent blasting consultant during the first 12 months of operation in order to obtain sufficient quarry data to confirm the initial guideline parameters and assist in refining future blast designs.
- 2. All blasts shall be monitored for both ground vibration and overpressure at the closest privately owned sensitive receptors adjacent the site, or closer, with a minimum of two (2) instruments one installed in front of the blast and one installed behind the blast.
- 3. Blasts shall be designed to maintain vibrations below 13mm/s at the location of the closest identified active spawning bed as per DFO guidelines. When blasting during active spawning season, a minimum of one supplemental vibration monitor shall be installed on the shoreline closest to the spawning bed to confirm the vibration levels.
- 4. The guideline limits for vibration and water overpressure shall adhere to standards as outlined in the Guidelines For the Use of Explosives In or Near Canadian Fisheries Waters (1998) or any such document, regulation or guideline which supersedes this standard.
- 5. All blasts shall be monitored for ground vibration at the adjacent TC Energy High Pressure Natural Gas Pipeline when blasting within 100m of the pipeline or when calculations suggest vibrations in excess of 35mm/s.
- 6. Blasts shall be designed to maintain vibrations at the transmission towers in the Hydro One Corridor below 50mm/s or any such document, regulation or corporate policy in effect at the time. When vibration calculations suggest vibrations at the towers may exceed 35mm/s, the towers shall be monitored for ground vibration.
- 7. Blasts shall be designed to maintain vibrations at the 4832 Thorold Townline Road utility buildings below 50mm/s. When vibration calculations suggest vibrations at the utility buildings may exceed 35mm/s, the buildings shall be monitored for ground vibration.
- 8. The guideline limits for ground vibration and air overpressure shall adhere to standards as outlined in the Model Municipal Noise Control By-law



- publication NPC 119 (1978) or any such document, regulation or guideline which supersedes this standard.
- 9. Orientation of the aggregate extraction operation will be designed and maintained so that the direction of the overpressure propagation will be away from structures as much as possible.
- 10. Blast designs shall be continually reviewed with respect to fragmentation, ground vibration and overpressure. Blast designs shall be modified as required to maintain compliance with current applicable guidelines and regulations.
- 11. Detailed blast records shall be maintained in accordance with current industry best practices.

The blast parameters described within this report are supported by the modelling in the attached appendices. As the quarry progresses and as site-specific data is collected from the on-going operation, the blast parameters can be refined, as necessary, to maintain continual compliance with MECP Guidelines.



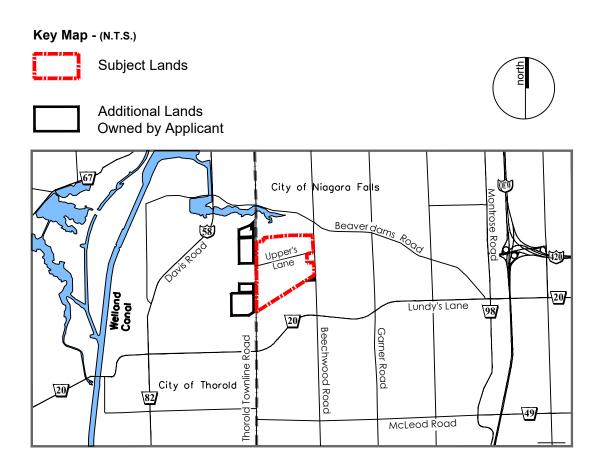
### CONCLUSION

The blast parameters described within this report will provide a good basis for the initial blasting operations at this location. As site specific blast vibration and overpressure data becomes available, it will be possible to refine these parameters on an ongoing basis.

Blasting operations required for operations at the proposed Uppers Quarry site can be carried out safely and within governing guidelines set by the Ministry of the Environment, Conservations and Parks.

Modern blasting techniques will permit blasting to take place with explosives charges below allowable charge weights ensuring that blast vibrations and overpressure will remain minimal at the nearest receptors.

# Appendix A



A. General

 This Site Plan is prepared under the Aggregate Resources Act for a Class A Licence for a quarry below the ground water table.

 2. Area to be licenced
 103.6 ha. (±256.0 ac.)

 Area to be extracted
 89.1 ha. (±220.2 ac.)

B. References

 Contour information was obtained from a topographic survey prepared by TEC Engineering (formerly Renishaw (Canada) Limited) using October 2016 and February 2017 aerial photography and are displayed in one metre intervals. Elevations shown are in metres above sea level (masl).

 Topographic information was obtained from numerous sources including Ontario GeoHub (Land Information Ontario), Google Earth Pro aerial photography captured on July 18, 2018 and field investigations for technical reports.

 All topographic features and structures are shown to scale in Universal Transverse Mercator (UTM) with North American Datum 1983 (NAD83), Zone 17 (metre), Central Meridian 81 degrees west coordinate system.

4. Property boundaries were obtained from a Plan of Survey prepared by Matthews,

Cameron, Heywood-Kerry T. Howe Surveying Ltd. dated April 5, 2012. Other property boundaries were established using Municipal Property Assessment Corporation (MPAC) parcel fabric data.

5. Zoning categories on or within 120 metres of the licence boundary are from the City of Niagara Falls Zoning By-law No. 79-200 (Schedules A3 and A4 - Consolidation April 2015).

6. Land use information on or within 120 metres of the licence boundary has been compiled from October 2016 orthophotography, site visits and water well survey data.

1. The maximum predicted water table is 184.9 masl and the contact aquifer

"Proposed Upper's Quarry - Maximum Predicted Water Table Report", dated October 2021.

D. Drainage1. Existing surface water drainage on and within 120 metres of the licence boundaries

potentiometric contours ranges between 176.0 and 184.9 masl (as per WSP's

are by overland flow in the direction shown by arrows on the plan view.

F. Significant Features

E. Site Access and Fencing1. There are two (2) existing site accesses on Thorold Townline Road, six (6) existing

site accesses on Upper's Lane, and three (3) existing site accesses on Beechwood

Post and wire fencing (unless otherwise noted) exists in the locations shown on the plan view.

All significant natural features on and within 120 metres of the licence boundary are shown on the Key Natural Heritage Features Schematic on this drawing.

shown on the Key Natural Heritage Features Schematic on this drawing.All significant human-made features on and within 120 metres of the licence boundary are shown on the plan view.

## G. Aggregate Related Site Features

1. There are no existing aggregate operations or features within the licence boundaries such as stationary or portable equipment, stockpiles, recyclable materials, scrap, fuel storage, haul roads, berms or excavation faces.

H. Technical Reports - References
1. Upper's Quarry: Acoustic Assessment Report, RWDI, October 2021 August 2, 2023.

 Agricultural Impact Assessment for Upper's Quarry, Colville Consulting Inc., October 2021.

3. Upper's Quarry: Air Quality Assessment, RWDI Air Inc., October 2021 July 12, 2023.
4. Archaeological Assessments:

 a. Stage 1 Archeological Resource Assessment of Walker Aggregates Proposed South Niagara Quarry, Part of Lots 102, 119, 120, 136 & 137, Archeological Services Inc., December 2008.

b. Stage 1-2 Archeological Assessment of Part 9764 Uppers Lane, Part of Lots 119 & 120, Archeological Assessments Ltd., November 3, 2005.

c. Stage 2-3 Archeological Assessment, Part of Lots 102, 119, 120, 136 & 137, Archeological Assessments Ltd., November 21, 2012.
d. Stage 1-2 Archeological Assessments, Upper's Quarry Additional Lands, Part of

Lots 119& 120, Archaeological Research Associates Ltd., April 20, 2020.
e. Stage 3 Mitigation of Development Impacts, Final Excavation Report, Walker XI (AgGT-411), Upper's Quarry, Archaeological Research Associates Ltd., May 26,

f. Stage 4 Mitigation of Development Impacts, Final Excavation Report, Walker XI (AgGT-178), Upper's Quarry, Archeological Research Associates Ltd., July 22,

5. Blast Impact Analysis, Upper's Quarry, Explotech, October 2021 August 2023.

Cultural Heritage Impact Assessment Report, Proposed Upper's Quarry, MHBC, October 2021.

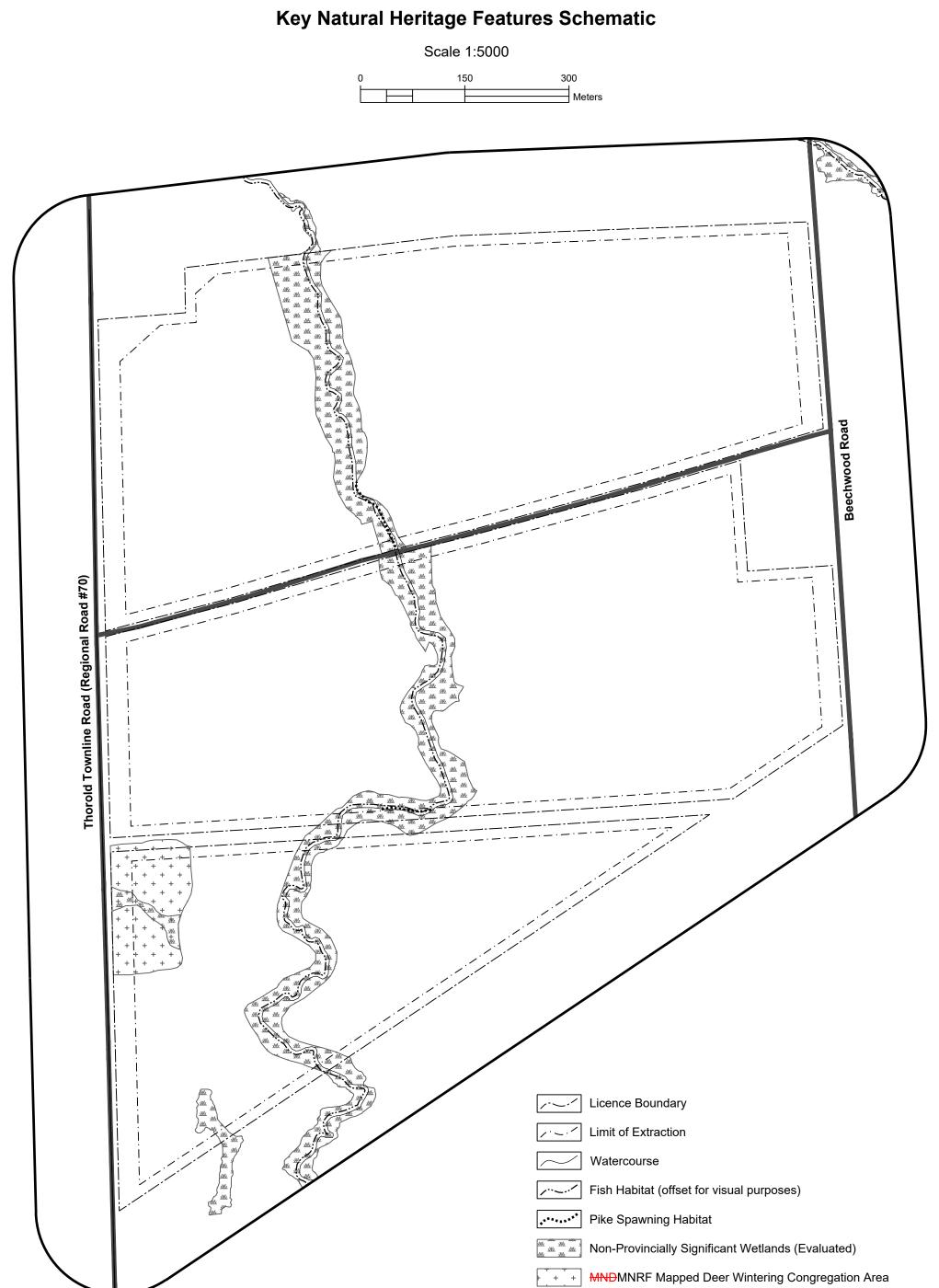
Economic Benefits Analysis, Prism, October 2021 February 2023.
 Level 2 Water Study Report and Response to JART Hydrogeological Comments,

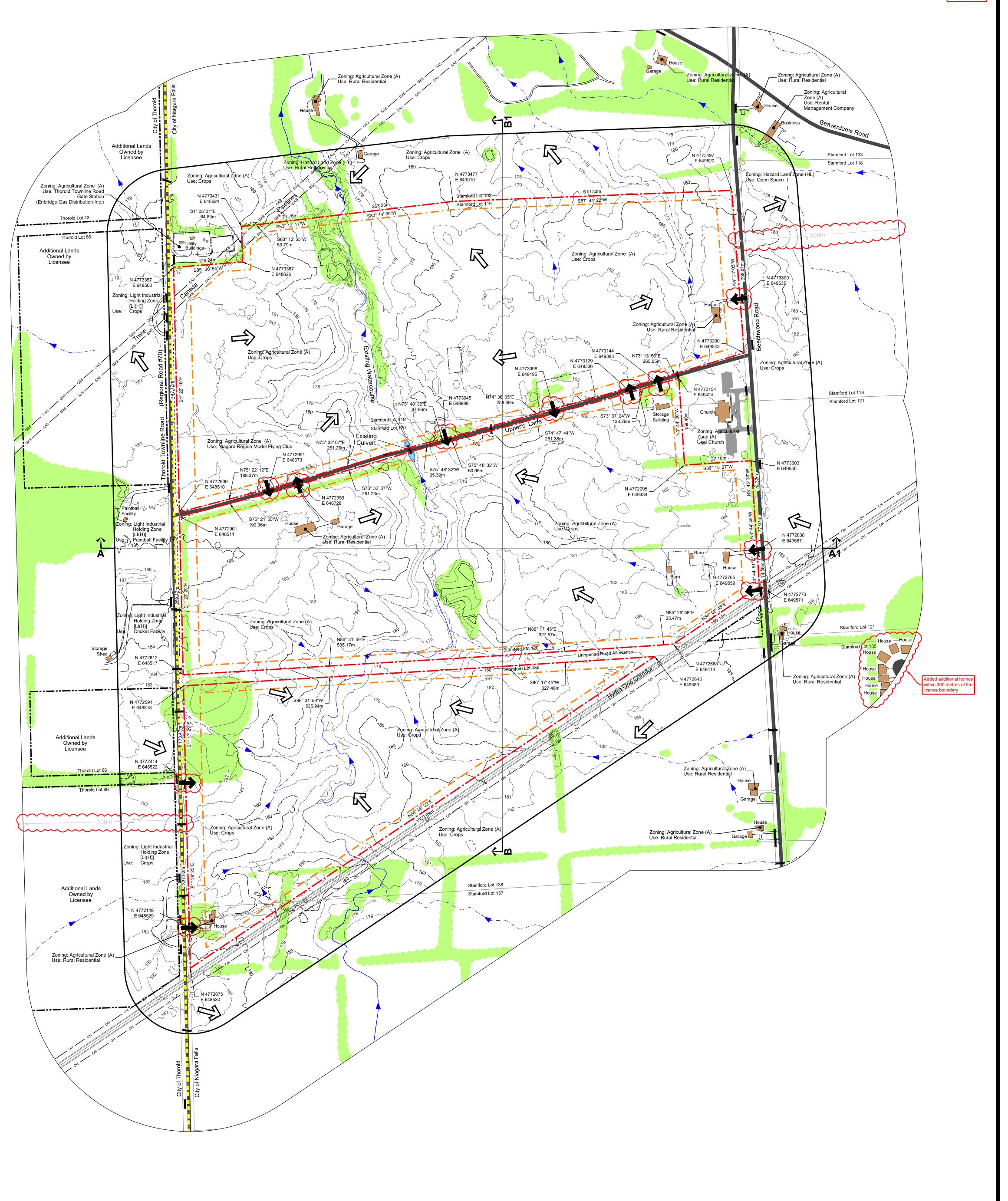
WSP, October 2021 October 3, 2022.9. Maximum Predicted Water Table Report, WSP, October 2021.

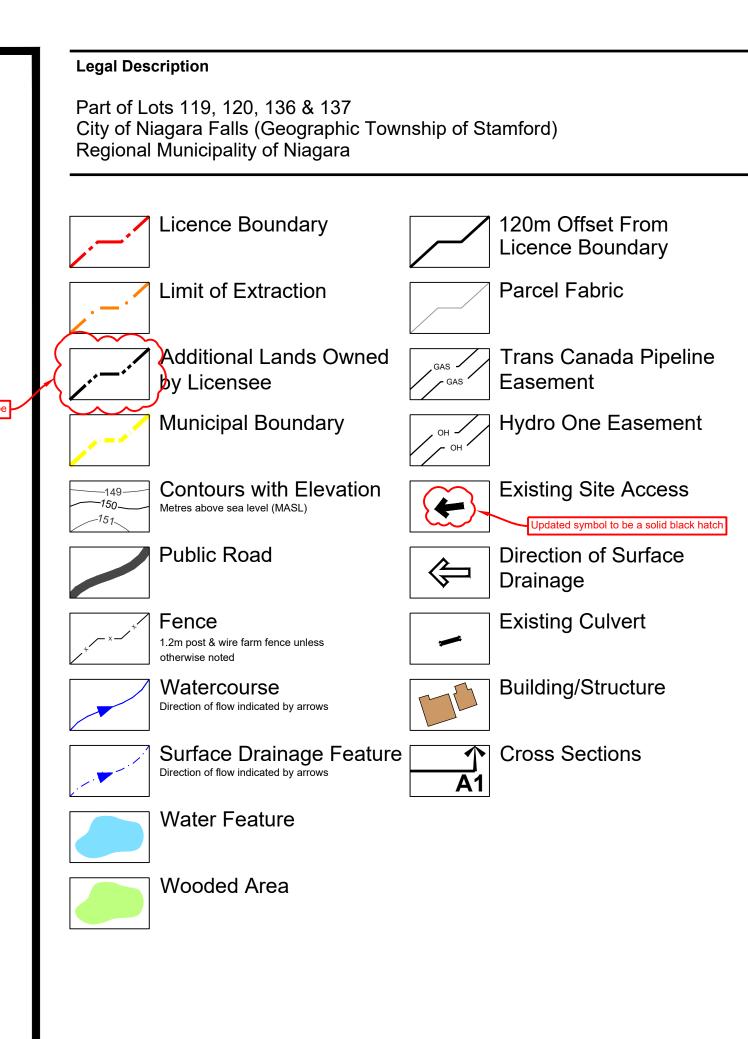
10. Upper's Quarry, Niagara: Level 1 and Level 2 Natural Environment Technical Report and Environmental Impact Study, Stantec, October 2021 August 2023.
11. Planning Justification Report and Summary Statement, MHBC, October 2021 August

12. Traffic Impact Study and TIS Addendum, Upper's Quarry, TMIG TYLin, October 2021

13. Visual Impact Assessment, Proposed Upper's Quarry, MHBC, October 2021.







## Site Plan Acronyms

- ARA Aggregate Resources Act
- 2. MNDMNRF Ministry of Northern Development, Mines, Natural Resources and Forestry
- 3. MHSTCI Ministry of Heritage, Sport, Tourism and Culture Industries
- MECP Ministry of the Environment, Conservation and Parks
   MGCS Ministry of Government and Consumer Services
- 6. DFO Department of Fisheries and Oceans Canada
- 7. ECA Environmental Compliance Approval
- 8. BMPP Best Management Practices Plan9. PTTW Permit to Take Water
- 10. MASL Metres above sea level
- 11. TCPL Trans Canada Pipeline
- 12. ROW Right of way13. HMA Hot mix asphalt
- 14. PWQO Provincial Water Quality Objectives
- 15. MISA Municipal Industrial Strategy for Abatement

16. TSS - Total Suspended Solids



walker aggregates

Walker Aggregates Inc. 2800 Thorold Townline Road P.O. Box 100 Thorold, Ontario L2V 3Y8

# Upper's Quarry

Plan Scale: 1:3000 (Arch E)

Outober 2021

Drawn By C.P. File No.

Checked By D.W.

Plan Scale: 1:3000 (Arch E)

Existing Features

1 of 6

Path N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan.dwg

# A. General

103.6 ha. (±256.0 ac.) Area to be licenced

Area to be extracted 89.1 ha. (±220.2 ac.)

- 2. The maximum amount of aggregate to be removed from this site in any calendar year is 1,800,000 tonnes.
- 3. In the event that Walker obtains permission from the City of Niagara Falls to extract the road allowance(s), the licensee may apply to the MNDMNRF to amend the licence and site plan to expand the licence boundary to include the road allowance directly adjacent to the licence boundary (i.e. Upper's Lane and/or the road allowance between Lots 120 and 136). An expansion to the licence boundary for this purpose will not require a new licence
- 4. All technical reports have taken into consideration the potential removal of the road allowance(s).
- Table 1 on this drawing identifies the number of sensitive receptors within 500 metres of the licence boundary and the distance from the licence boundary to each receptor.

### B. Hours of Operation

1. The proposed quarry will have the following hours of operation:

under Section 7 of the Aggregate Resources Act (ARA).

Activity	Monday to Friday	Saturday	Sunday	
Drilling, extraction (at working face)	7:00 am to 7:00 pm	7:00 am to 7:00 pm	N/A	
Blasting	8:00 am to 6:00 pm	N/A	N/A	
Aggregate processing at mobile crusher plant	7:00 am to 7:00 pm	7:00 am to 7:00 pm	N/A	
Asphalt plant operations	24 hours per day	24 hours per day	24 hours per day	
Internal hauling of aggregate and/or recycled material:				
<ul> <li>From working face (shot rock) to mobile crusher plant</li> </ul>	7:00am to 7:00pm	7:00am to 7:00pm	N/A	
- From mobile crusher plant/stockpiles to asphalt plant	24 hours per day	24 hours per day	24 hours per day	
Aggregate and recycling shipping to and/or from the quarry (including hot mix asphalt shipping from quarry and receiving recycled asphalt to quarry)	24 hours per day	24 hours per day	24 hours per day	
Maintenance	24 hours per day	24 hours per day	24 hours per day	
Conveyor to the mobile crusher plants	7:00 am to 7:00 pm	7:00 am to 7:00 pm	N/A	

No operations shall occur on Statutory Holidays except as noted below. A response to emergencies is not limited by the hours of operations shown on this plan.

### C. Proposed Entrances/Exits and Fencing

- 1. For the Mid Extraction Area:
- a. All traffic for operations will enter and exit the Mid Extraction Area from Upper's Lane using a main entrance/exit in the location generally shown on the plan view.
- b. If an entrance/exit off of Upper's Lane is not permitted, traffic for operations will enter and exit the Mid Extraction area from Thorold Townline Road. If approved, the site plan will be updated to accurately depict the location of the entrance/exit off of Thorold Townline Road.

### 2. For the South Extraction Area:

- a. Material will be transported to the Mid Extraction Area for processing via a conveyor over the unopened road allowance between Lots 120 and 136. Limited traffic required for operations will enter and exit the South Extraction Area via a crossing over the unopened road allowance between Lots 120 and 136, subject to approval from the City, in the location generally shown on the plan view.
- If permission to cross the unopened road allowance is not granted, traffic for operations will enter and exit the South Extraction area from Thorold Townline Road. If approved, the site plan will be updated to L. Spills Plan
- 3. For the North Extraction Area:
  - a. All traffic for operations will enter and exit the North Extraction Area from Upper's Lane using a main entrance/exit in the locations generally shown on the plan view.
  - b. If an entrance/exit off of Upper's Lane is not permitted, traffic for operations will enter and exit the North Extraction area from Thorold Townline Road. If approved, the site plan will be updated to accurately depict

4. Only one operational entrance/exit will be utilized at any one time.

the location of the entrance/exit off of Thorold Townline Road.

accurately depict the location of the entrance/exit off of Thorold Townline Road.

non-operation and shall be maintained throughout the life of the licence. 6. The licence boundaries shall be fenced in the locations shown on the plan view (prior to the commencement of

5. Once established, each operational entrance/exit shall be gated. All gates shall be kept closed during hours of

operations) and shall be maintained for the life of the licence with upkeep during periodic inspections (see Section

## N Variations from Control and Operation Standards on this drawing).

D. Drainage and Siltation Control

1. Silt fencing/sediment control measures will be installed within the Watercourse Realignment Transition Area prior to extraction in each extraction area and along the easterly and northerly limits of Phase 1B after the watercourse

# E. Site Preparation

- 1. All existing structures within the licence boundary shall be demolished or removed (and any associated residential entrances closed off) prior to extraction in each extraction area. Prior to erecting or demolishing a building, all necessary Permits shall be obtained by the City in accordance with the Ontario Building Code Act, to the satisfaction of the Building Services Division and the Fire Prevention Division.
- . Timber resources (if any) will be salvaged for use as saw logs, fence posts and fuel wood where appropriate. Stumps and brush cleared will be burned (with applicable permits), used for shoreline habitat enhancement or mulched for use in progressive rehabilitation.
- Areas of the site will be stripped of topsoil/overburden in stages in accordance with the phases. Topsoil and overburden will be stripped and stored in berms and/or stockpiles wherever feasible.
- 4. Topsoil and overburden shall be placed in perimeter acoustic/visual berms, pond construction, watercourse realignment or used immediately for progressive rehabilitation in this licence or existing Licence Numbers 11175
- . Excess topsoil and overburden not required for immediate use in berms or rehabilitation may be temporarily stockpiled on the quarry floor. Topsoil and overburden stockpiles shall be located within the limit of extraction and

and 4437 (see Section N Variations from Control and Operation Standards on this drawing).

- remain a minimum of 30 metres from the licence boundary and 90 metres from a property with a residential use.
- Temporary topsoil and overburden stockpiles which remain for more than one year shall have their slopes vegetated to control erosion. Seeding shall not be required if these stockpiles have vegetated naturally in the first

# F. Setbacks, Berms and Screening

- Setbacks are as shown on the plan view. Excavation will occur within the extraction setback area along the west and northwest area of the licensed boundary to accommodate grading required for the realignment of the existing watercourse. Furthermore, areas within the setbacks will be accessed as necessary to perform general site servicing, maintenance (berming, fencing etc.) and progressive rehabilitation. See Section N Variations from Control and Operation Standards on drawing 2 of 6.
- Locations and heights for all acoustic/visual berms are provided on the plan view. All proposed berms shall be constructed in accordance with the "Typical Acoustic Berm Detail" (on this drawing), "Typical Visual Berm Detail" (on drawing 4 of 6) and, more specifically, berms adjacent to Beechwood Road will be constructed in accordance N. Variations from Control and Operation Standards with "Typical Berm - Adjacent to Beechwood Berm Detail" (on this drawing). Where the proposed berm transects the existing watercourse along the north perimeter, a culvert shall be installed in accordance with DFO requirements. Culverts will also be installed under berms, where necessary, to maintain existing drainage to and from off-site and to the existing watercourse. All proposed berms and will be vegetated with non-invasive plant species and maintained to control erosion. Temporary erosion control will be implemented as required.
- 3. Perimeter acoustic berms may be removed for final rehabilitation in the final Phase when they are no longer required for noise attenuation.

### 4. Any natural treed buffer areas in the setbacks will be maintained where feasible subject to berm requirements. G. Site Dewatering

water will be discharged from the sumps to the realigned watercourse in Phase 1B.

- 1. Surface water will be discharged from the sump areas to the existing watercourse until the watercourse is realigned to the location of Phases 1B and 2B. Once the watercourse realignment has been completed, surface
- Sump: During quarry development, a portable submersible pumps will be installed in each Initial Sinking Cut Area for the purpose of dewatering to maintain a dry working area and/or aggregate washing. Water will be pumped from the sumps to a pond where it is either used for aggregate washing or discharged to the existing watercourse. The sumps shall be relocated (as required) within each extraction area during the operational life of the guarry.
- H. Extraction Details
- 1. The extraction sequence is outlined on drawing 3 of 6.
- 2. The proposed maximum depth of extraction is indicated by the spot elevations shown on the plan view. Extraction shall proceed to a maximum depth of approximately 42 m below ground surface (ranging in elevation from 141 masl in the southwest to 149 masl in the northeast portions of the site), corresponding to the geologic base of the Gasport dolostone of the Lockport Group.

For the "Watercourse Realignment Transition Area", the maximum depth of extraction is approximately 1 metre (down to an elevation of 174 masl) and any extraction in the "Watercourse Realignment Transition Area" shall be

- completed as part of site preparation (construction of compensatory ponds). No drilling or blasting shall be permitted in the "Watercourse Realignment Transition Area".
- . Internal haul road locations shall vary as extraction progresses and will be located on the quarry floor with the exception of at grade crossings.

Blasted aggregate will be transported back to the mobile crusher plant and processing area on the quarry floor for

- processing and shipping. . An office/scale house and weigh scale will be established on site. A maintenance shop and shed(s) may be constructed on site. Portable office/storage trailers and structures associated with fuel storage may be brought
- onto the site for temporary periods for uses associated with quarry activity. All structures shall remain 30 metres from the licence boundary / Trans Canada Pipelines easement or 90 metres from the licence boundary if the boundary abuts land that is used for residential purposes or is restricted to residential use by the Zoning By-law at the time the licence is issued. Aggregate stockpiles (including recyclable material) shall be located within the limits of extraction and remain a
- minimum of 30 metres from the licence boundaries (except where the licence boundaries abut Upper's Lane and the unopened road allowance - See Section N Variations from Control and Operation Standards on this drawing) and 90 metres from a property with a residential use.

# Equipment and Processing

- 1. A portable processing plant (including primary, secondary and tertiary crushing and screening units) will be permitted within the North and Mid Extraction Areas inclusive.
- 2. Processing shall be located within the limit of extraction and remain a minimum of 30 metres from the licence boundary and 90 metres from a property with a residential use.
- 3. During the sinking cuts and early phases of operation, the primary crusher will be integrated into a single processing plant located near the working face. In later phases, the primary crusher will split from the single integrated plant and start to follow the working face. The processing plant, which contains the secondary and tertiary crushers, will remain close to the quarry entrance shall be placed in the location identified on the Extraction Sequence Schematic on drawing 3 of 6 during each stage of extraction. The processing plant will be located at varying elevations, beginning at the top of rock during the sinking cut portion of operations, and moving to the first bench and then the final quarry floor as space becomes available. See note A.3. on drawing 4 of 6 for additional information.

- 4. Once processing has progressed to Phase 2A, a hot mix asphalt (HMA) batch plant facility shall be established on the quarry floor (in the location shown on the plan view) in Phase 1A. The HMA batch plant shall remain in the location shown on the plan view for the life of the quarry until extraction is complete and shall be removed during progressive rehabilitation.
- 5. In Phase 4, the portable processing plant shall require additional shielding in accordance with note A.5 on drawing 4 of 6.
- 6. A wash plant and temporary wash ponds may be established and located to move together with the portable processing plant, subject to permit approval from MECP.
- 7. Equipment to be used onsite may include, but shall not be limited to:

## a. Working Face - 1 silenced rock drill; 1 loader;

- b. Processing 1 portable processing plant including crushers, screeners, and stackers; 2 loaders (at
- c. Asphalt 1 asphalt plant; 2 loaders, 1 compressor vent, 1 dust controller blower (motor and stack); elevator motor, conveyor motor, oven motor, pug mill (door and motor);
- d. Conveyor(s);

J. Frequency / Timing of Blasts

drawing 4 of 6.

requirements.

- e. Generator(s) (diesel-fueled); and
- f. Rock trucks, haul trucks, shipment trucks and fuel trucks.
- 8. If required, an Environmental Compliance Approval will be obtained for processing equipment to be used on-site. 8. Wash pond(s) and sump(s) may be permitted in accordance with Environmental Compliance Approval or Permit to Take Water Requirements. The pond(s) and sump(s) will move throughout operations and as extraction
- progresses horizontally and vertically.
- 9. Equipment used for construction of the perimeter berms/barriers, overburden stripping, rehabilitation, the new watercourse corridor, as well as other quarry related construction projects will be utilized on site.
- 1. Prior to blasting being permitted within the <del>100</del> 300 metre setback of the TransCanada Pipeline, identified as 'TransCanada Blasting Buffer Area' on this Plan, the licensee shall address the requirements of notes D.5 on
- 2. All blast monitoring reports shall be retained by the licensee for a period of seven years after each blast and made available upon request for audit purposes. See Section D on drawing 4 of 6 for detailed blasting

## K. Fuel Storage

- Fuel storage tanks will be located in close proximity to the main processing plant (or in an alternative location subject to approval by the MNDMNRF). Fuel storage tanks shall be installed and maintained in accordance with Technical Standards and Safety Act, 2000. Liquid Fuels Handling Code, 2000 and Liquid Fuels Regulation Reg.
- 2. All fuel tanks shall be doubled sided or placed in containment facilities large enough to hold the tanks maximum
- 3. Fuel trucks shall be used to transfer fuel to on-site equipment in accordance with the Liquid Fuels Handling Code,
- 4. A Spills Contingency Plan shall be prepared and implemented prior to site preparation. The Spills Contingency Plan shall be available on site and all employees and contractors shall be informed and required to comply with

- a. The Ministry of Environment, Conservation and Parks (MECP) (see address and phone number below) and surrounding landowners will be notified.
- b. For a leakage or spill, immediate action will be taken to stop it. At the same, measures will be taken to prevent spreading. These measures may include building a berm or construction of a ditch, for instance. c. The quarry operator shall commence recovery procedures by collecting the spilled substance into
- d. The soil in the area affected by the spill or leak shall be removed and disposed of at a location prescribed

# Ministry of Environment, Conservation and Parks

Niagara District Office Garden City Tower 9th Floor Suite 15 301 St. Paul Street

St. Catharines, Ontario

### Spills Action Centre: 1-800-268-6060 M. Scrap and Recycling

- 1. Scrap may be stored on-site and shall be removed on an on-going basis.
- 2. Scrap shall only include material generated directly as a result of the aggregate operation such as refuse, debris, scrap metal, lumber, discarded machinery, equipment and motor vehicles.
- 3. All fluids shall be drained from any discarded equipment, machinery or motor vehicle prior to storage and disposed of in accordance with the Environmental Protection Act.
- Scrap shall not be stored within 30 metres of any body of water or the licence boundary and shall be kept in close proximity to the main processing plant.
- 5. Recycling of asphalt, concrete, porcelain and glass shall be permitted on-site.
- 6. Recyclable asphalt materials shall not be stockpiled within: 6.1. 30 metres of any waterbody or man-made pond; or
- 6.2. 2 metres of the ground water table.
- Recyclable material shall be kept in close proximity to the main processing plant and shall be stored separately on the guarry floor and within the extraction area limit.
- Rebar or other structural metal shall be separated from recyclable aggregate material during processing and placed in a designated scrap pile on-site which shall be removed on an on-going basis.
- 9. Recycled aggregate shall be removed on an on-going basis.
- 10. Recycling activities shall not interfere with the operational phases of the site or with rehabilitation.
- 11. Once the site is depleted, no further importation of recyclable material shall be permitted. Once final rehabilitation has been completed and approved in accordance with the site plan, all recycling
- operations shall cease. 13. The site shall be kept in an orderly condition.

	Variations from Control and Operation Standards						
No.	Variation	Rationale	Standar (0.13)				
1	Extraction shall occur within 30 metres but no closer than 15 metres from the Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136.  In addition, as part of construction of any access shown on the Site Plan and the existing watercourse realignment, extraction may occur:  - Within the 15 metre setback from the Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136 for access purposes,  - Within the 15 metre setback from the north and south boundaries of the site for riparian corridor construction and  - Within the 30 metre setback from Thorold Townline Road for riparian corridor construction.	Upper's Lane and the unopened road allowance are isolated since no road allowance exists for either to the west of Thorold Townline Road or east of Beechwood Road.  Setbacks will be disturbed in order to facilitate construction associated with the site access points and watercourse realignment.	(1) 9 ar 10				
2	Overburden may be removed from the extraction setback area to permit:  - Extraction within 30 metres but no closer than 15 metres from Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136  Overburden and aggregate may be removed from the excavation setback areas to permit the construction of any access or to implement the existing watercourse realignment as follows:  - Within the 15 metre setback from the Upper's Lane road allowance and the unopened road allowance between Lots 120 and 136 for access purposes,  - Within the 15 metre setback from the north and south boundaries of the site for riparian corridor construction and  - Within the 30 metre setback from Thorold Townline Road for riparian corridor construction.	Upper's Lane and the unopened road allowance are isolated since no road allowance exists for either to the west of Thorold Townline Road or east of Beechwood Road.  Setbacks will be disturbed in order to facilitate construction associated with the site access points and watercourse realignment.	(1) 11				
3	Topsoil and overburden may be moved between this Licence and Licence Numbers 11175 & 4437. to provide for effective rehabilitation of these licences.	This will provide for effective rehabilitation of these licences.	(1) 18				
4	A portion of the quarry face shall remain vertical. See Rehabilitation Plan, drawing 5 of 6.	Vertical faces above and below the lake level will create a more diverse habitat and visually appealing rehabilitated landform.	(1) 19				
5	The licence boundary for the North Extraction Area shall not be fenced on or west of the Trans Canada Pipeline easement. Fencing shall be erected on the eastern extent of the easement.	This will allow Trans Canada to have unobstructed access to the easement for maintenance purposes.	(3)(a)				

# O. Trans Canada Pipeline (TCPL)

1. The licencee shall notify TCPL if it intends to blast within 300 metres of their right-of-way (easement). No blasting shall occur until written consent is obtained from TCPL.

3. Crossing of the TCPL right-of-way with vehicles is not permitted without written consent from TCPL.

accessory buildings shall be located a minimum of 3 metres from the edge of the right-of-way.

- 2. Any other work (other than blasting) within 30 metres of TCPL's right-of-way requires written consent from TCPL.
- 4. No material extraction shall be permitted within 40 metres of TCPL's right-of-way without written consent from the Canada Energy Regulator (CER), formerly NEB or National Energy Board.
- . No buildings or structures shall be constructed anywhere on TCPL's right-of-way. Permanent buildings and structures shall be located a minimum of 7 metres from the edge of the TCPL right-of-way. Temporary or
- A minimum setback of 7 metres from the nearest portion of a TCPL pipeline right-of-way shall also apply to any parking area or loading area, including any parking spaces, loading spaces, stacking spaces, bicycle parking spaces, and any associated drive aisle or driveway.

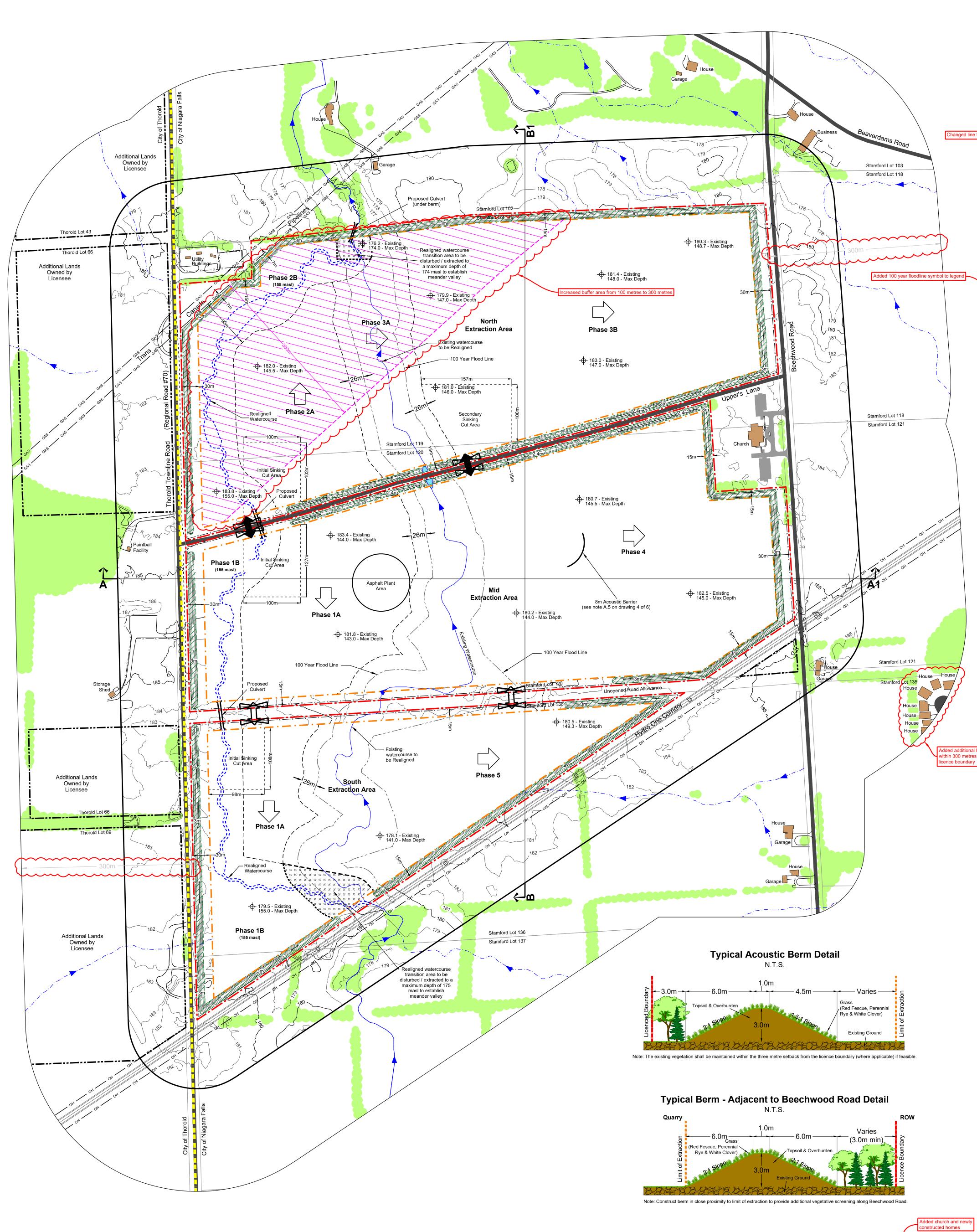


Table 1: Sensitive Receptors Within 500m of the Licence Boundary																	
Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address	Distance	Receptor	Address	Distanc
101	10148 Beaverdams Road	184 m	121	5695 Osprey Avenue	374 m	141	9349 Madison Crescent	415 m	161	9245 Shoveller Drive	489 m	181	9414 Shoveller Drive	416 m	201	9461 Eagle Ridge Drive	427 m
102	10138 Beaverdams Road	442 m	122	5687 Osprey Avenue	362 m	142	9337 Madison Crescent	423 m	162	9245 Shoveller Drive	495 m	182	9404 Shoveller Drive	423 m	202	9500 Eagle Ridge Drive	474 n
103	9722 Beaverdams Road	234 m	123	5679 Osprey Avenue	350 m	143	9325 Madison Crescent	434 m	163	9312 Madison Crescent	417 m	183	9394 Shoveller Drive	428 m	203	9494 Eagle Ridge Drive	477 r
104	9582 Beaverdams Road	151 m	124	5671 Osprey Avenue	339 m	144	9315 Madison Crescent	445 m	164	9324 Madison Crescent	404 m	184	9374 Shoveller Drive	443 m	204	9490 Eagle Ridge Drive	478 r
105	9417 Beaverdams Road	447 m	125	5663 Osprey Avenue	333 m	145	9245 Shoveller Drive	469 m	165	9336 Madison Crescent	390 m	185	9364 Shoveller Drive	450 m	205	9484 Eagle Ridge Drive	480 r
106	9337 Beaverdams Road	475 m	126	5655 Osprey Avenue	321 m	146	9245 Shoveller Drive	461 m	166	9352 Madison Crescent	370 m	186	9354 Shoveller Drive	460 m	206	9440 Eagle Ridge Drive	484 r
107	5584 Beaverdams Road	81 m	127	5647 Osprey Avenue	311 m	147	9245 Shoveller Drive	453 m	167	9366 Madison Crescent	354 m	187	9344 Shoveller Drive	467 m	207	9440 Eagle Ridge Drive	495 r
108	5769 Beaverdams Road	287 m	128	5639 Osprey Avenue	299 m	148	9245 Shoveller Drive	447 m	168	9380 Madison Crescent	338 m	188	9334 Shoveller Drive	478 m	208	5772 Osprey Avenue	499 ו
109	5821 Beaverdams Road	360 m	129	5631 Osprey Avenue	290 m	149	9245 Shoveller Drive	440 m	169	5610 Osprey Avenue	311 m	189	9324 Shoveller Drive	488 m	209~	9440 Eagle Ridge Drive	4947
110	5783 Osprey Avenue	490 m	130	5623 Osprey Avenue	284 m	150	9245 Shoveller Drive	410 m	170	5622 Osprey Avenue	323 m	190	9314 Shoveller Drive	494 m	210	5599 Osprey Avenue	251 ו
111	5775 Osprey Avenue	480 m	131	5615 Osprey Avenue	271 m	151	9245 Shoveller Drive	425 m	171	5632 Osprey Avenue	331 m	191	9355 Eagle Ridge Drive	494 m 🕻	211	9457 Madison Crescent	260
112	5767 Osprey Avenue	470 m	132	5607 Osprey Avenue	259 m	152	9245 Shoveller Drive	435 m	172	5642 Osprey Avenue	341 m	192	9365 Eagle Ridge Drive	481 m	212	5329 Beechwood Road	63 r
113	5759 Osprey Avenue	459 m	133	9445 Madison Crescent	280 m	153	9245 Shoveller Drive	443 m	173	5652 Osprey Avenue	350 m	193	9375 Eagle Ridge Drive	469 m	<del>\</del>		<del></del>
114	5751 Osprey Avenue	448 m	134	9433 Madison Crescent	299 m	154	9245 Shoveller Drive	457 m	174	5668 Osprey Avenue	362 m	194	9385 Eagle Ridge Drive	471 m			
115	5743 Osprey Avenue	438 m	135	9421 Madison Crescent	316 m	155	9245 Shoveller Drive	467 m	175	9405 Shoveller Drive	374 m	195	9395 Eagle Ridge Drive	464 m			
116	5735 Osprey Avenue	424 m	136	9409 Madison Crescent	334 m	156	9245 Shoveller Drive	476 m	176	9395 Shoveller Drive	383 m	196	9045 Eagle Ridge Drive	457 m			
117	5727 Osprey Avenue	415 m	137	9397 Madison Crescent	351 m	157	9245 Shoveller Drive	485 m	177	9385 Shoveller Drive	392 m	197	9415 Eagle Ridge Drive	448 m			
118	5719 Osprey Avenue	404 m	138	9385 Madison Crescent	371 m	158	9245 Shoveller Drive	498 m	178	9446 Shoveller Drive	400 m	198	9425 Eagle Ridge Drive	445 m			
119	5711 Osprey Avenue	393 m	139	9373 Madison Crescent	391 m	159	9245 Shoveller Drive	474 m	179	9434 Shoveller Drive	405 m	199	9435 Eagle Ridge Drive	443 m			
120	5703 Osprey Avenue	383 m	140	9361 Madison Crescent	407 m	160	9245 Shoveller Drive	482 m	180	9424 Shoveller Drive	412 m	200	9445 Eagle Ridge Drive	436 m			

## **Legal Description** Part of Lots 119, 120, 136 & 137 City of Niagara Falls (Geographic Township of Stamford) Regional Municipality of Niagara 120m Offset From Licence Boundary Licence Boundary Trans Canada Blasting Limit of Extraction Buffer Area - See Note D.5 on drawing 4 of 6 Additional Lands Owned Parcel Fabric by Licensee Municipal Boundary | Easement \_\_\_\_\_ Contours with Elevation <sup>-150</sup> Metres above sea level (MASL) Entrance / Exit Limited Service Access For Phases 1A, 1B and 5 in South Extraction Area 1.2m post & wire farm fence unless otherwise noted Watercourse Direction of flow indicated by arrows Surface Drainage Feature Direction of flow indicated by arrows Watercourse - Realigned General Direction of (Stantec, 2020) Excavation & Boundary 100 Year Floodline Top - Noise Attenuation Berm Top - Noise Attenuation Bottom - Visual Berm Water Feature | Building/Structure Wooded Area Spot Elevation Metres above sea level (MASL) Bottom - Maximum Depth of Extraction Cross Sections Watercourse Realignment

# Site Plan Acronyms

- 1. ARA Aggregate Resources Act
- 2. MNDMNRF Ministry of Northern Development, Mines, Natural Resources and Forestry
- MHSTCI Ministry of Heritage, Sport, Tourism and Culture Industries
- 4. MECP Ministry of the Environment, Conservation and Parks 5. MGCS - Ministry of Government and Consumer Services
- 6. DFO Department of Fisheries and Oceans Canada
- 7. ECA Environmental Compliance Approval 8. BMPP - Best Management Practices Plan
- 9. PTTW Permit to Take Water
- 10. MASL Metres above sea level
- 11. TCPL Trans Canada Pipeline 12. ROW - Right of way
- 13. HMA Hot mix asphalt 14. PWQO - Provincial Water Quality Objectives
- 15. MISA Municipal Industrial Strategy for Abatement
- 16. TSS Total Suspended Solids





**Applicant** 

File Name

Walker Aggregates Inc. 2800 Thorold Townline Road P.O. Box 100 Thorold, Ontario L2V 3Y8

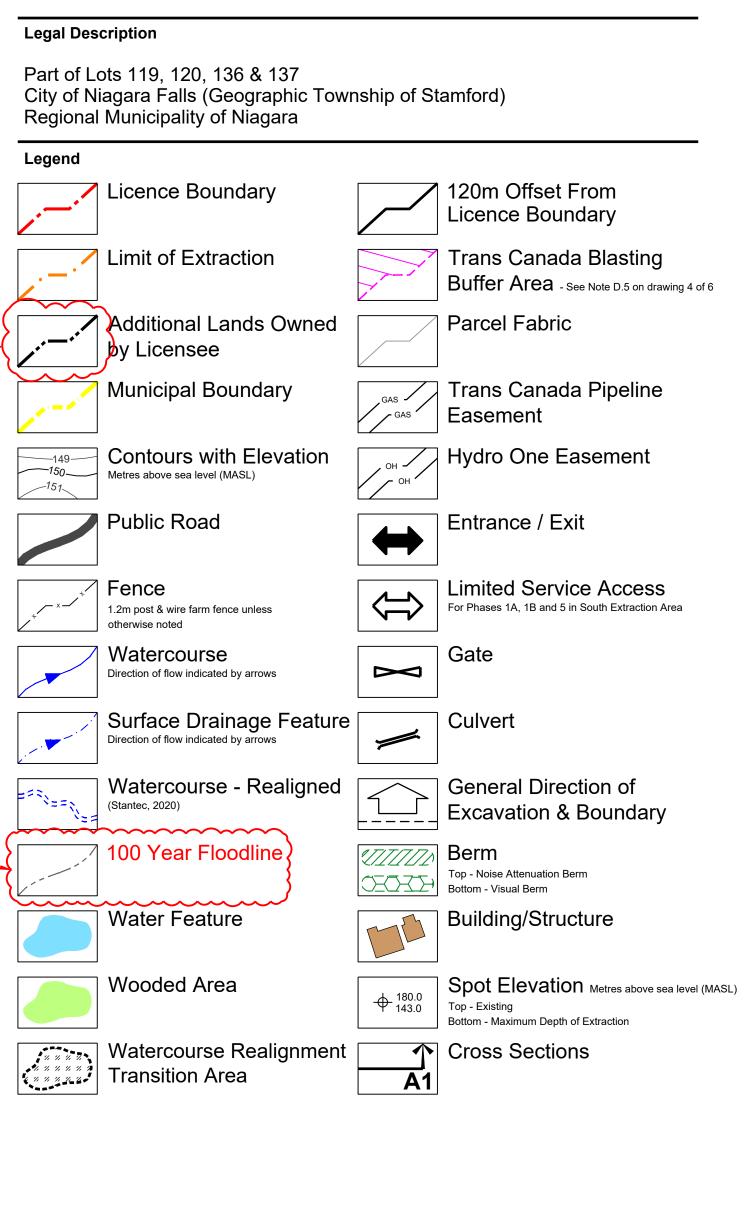
# Upper's Quarry

MNDMNRF Licence Reference No. **Applicant's Signature** Plan Scale: 1:3000 (Arch E) October 2021

**Operational Plan** Drawing No. 2 of 6

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### A. General 4. A portable pump shall be utilized as necessary to discharge water to a man-made pond for aggregate washing or to a sediment forebay before being discharged to the existing watercourse. During heavy rainfall events (25 mm 1. This plan depicts a schematic operations sequence for the property based on the best information available at the or more), the pump will be deactivated as necessary to prevent flooding along the watercourse downstream of the site. The discharge, pond and forebay locations will move with the quarry face until the final quarry depth is time of preparation. reached. At this point, a permanent sump will be established. 2. Phases do not represent any specific or equal time period. Similar to Phase 1, the new watercourse channel shall be constructed within Phase 2 running along the east side The direction of extraction will <del>generally</del> be in accordance with the General Direction of Excavation (shown on the of Thorold Townline Road (Phase 2B) for the eventual realignment of the existing watercourse. As resource plan view) unless otherwise authorized by MNRF. Notwithstanding the operational and rehabilitation notes, extraction is completed in Phase 2B, this area will be filled with clay overburden material from on-site to an elevation ranging between 173 to 178 masl. The new watercourse and riparian wetland channel will be demand for certain products, blending of materials or Water Study Contingency measures may require minor deviations in the extraction and rehabilitation sequence. Any major deviations from the operations sequence shall constructed, designed and vegetated in accordance DFO authorization and Rehabilitation Plan (drawing 5 of 6). require approval from the MNRF. The maximum combined disturbed area which includes the processing plant, As extraction reaches the final quarry floor, and there is sufficient separation from the quarry floor working areas berms, stockpiles, silt pond, active extraction area and area being stripped for the next area of extraction within the licence boundary identified on this Drawing but excludes the area of Phase 1A needed for the continued in Phase 2A, a 2:1 sideslope along the easterly and northerly limit of Phase 2B shall be backfilled with either: (i) operation of the asphalt plant for the life of the quarry. Concurrent extraction of phases is permitted for blending overburden stockpiled on-site; (ii) overburden in Phase 3B; or (iii) material imported from Licence Numbers 11175 purposes provided the overall maximum combined disturbed area does not exceed 40 hectares to ensure and 4437. progressive rehabilitation of the site is being undertaken as required by the Site Plans. 7. Commence site preparation of Phase 3. Progressive and final rehabilitation will be completed in direct correlation to the development of the quarry as the extraction limits are reached and enough area is available to ensure that rehabilitation activities will not interfere E. Phase 3 (3A & 3B) with the production, stockpiling and processing of aggregate materials. 1. Proceed with stripping of overburden/topsoil. B. Initial Site Preparation 2. Prior to undertaking any works within Phase 3A that may result in any serious harm to fish, according to 35(1) of 1. Generally, site preparation in Phases 1 and 2 to include but not limited to: the Fisheries Act, the Licensee shall obtain a Fisheries Act Authorization from the Department of Fisheries and Oceans (DFO) and shall fulfill any other conditions required by the DFO as stated on its authorization. Once obtained, a copy of the Fisheries Act Authorization shall be provided to the MNRF. Once the watercourse has a. Constructing the main entrance and cross over(s) in accordance with entrance permit approvals been realigned to the satisfaction of DFO, stripping of overburden and topsoil can proceed in Phase 3A. b. Establishing fencing around licenced boundary (see Section N Variations from Control and Operation Standards on drawing 2 of 6) 3. In the event that watercourse relocation has not been approved or completed, extraction in Phase 3B may proceed before extraction in Phase 3A. c. Removal of trees and existing buildings (in accordance with all site plan requirements and applicable 4. In the event that Phase 3B is extracted before Phase 3A, a portable pump shall be utilized as necessary to discharge water to a man-made pond for aggregate washing or to a sediment forebay before being discharged to d. Proceed with stripping of overburden/topsoil from Phase 1 and, if necessary, Phase 2 the existing watercourse. During heavy rainfall events (25 mm or more), the pump will be deactivated as necessary to prevent flooding along the watercourse downstream of the site. The discharge, pond and forebay e. Construction of berms/acoustic barriers within the perimeter setback of the licence boundary (as shown on locations will move with the quarry face until the final quarry depth is reached. At this point, a permanent sump the plan view). will be established. Additional Lands Owned by Stamford Lot 103 Licenseé Install water management and erosion and sediment control measures (silt fencing) in accordance with note D.1 5. Phase 3A and 3B shall be extracted in up to three (3) lifts to a depth ranging between 145 masl to 149 masl. Stamford Lot 118 on this drawing and note E.1.c on drawing 4 of 6. Extraction will proceed in an easterly direction, moving gradually from north to south. Commence portable crushing/screening plant set up. The plant shall operate in accordance with Section A on 6. Once the existing watercourse has been realigned, extraction in Phase 3A may proceed. drawing 4 of 6 for all Phases. Proposed Culvert 7. Continue progressive rehabilitation of the quarry perimeter where limits of extraction have been reached and C. Phase 1 (1A and 1B) there is sufficient separation from the quarry floor working areas. ded 100 year floodline symbol to legend 1. Commence extraction in the 'Initial Sinking Cut Area' identified in the Mid and South Extraction Area (see plan 8. Commence site preparation of Phase 4. Thorold Lot 43 ~~~~~ ++ 180.3 - Existing 148.7 - Max Depth F. Phase 4 2. Phase 1A shall be extracted in up to three (3) lifts to a depth ranging between 140 masl and 145 masl. Realigned watercourse 1. Proceed with stripping of overburden/topsoil. transition area to be disturbed / extracted to 3. Phase 1B shall be extracted in one (1) to two (2) lifts to a depth of 155 masl. Additional Lands a maximum depth of 2. Commence Phase 4 extraction in an easterly direction, moving gradually from north to south. 174 masl to establish Owned by A portable pump shall be utilized as necessary in the Mid Extraction Area and the South Extraction Area to meander valley discharge water to a man-made pond for aggregate washing or to a sediment forebay before being discharged to 3. Phase 4 shall be extracted in up to three (3) lifts to a depth ranging between 142 masl in and 147 masl. the existing watercourse. During heavy rainfall events (25 mm or more), the pump will be deactivated as 4. Continue progressive rehabilitation of the quarry perimeter where limits of extraction have been reached and necessary to prevent flooding along the watercourse downstream of the site. The discharge pond and forebay locations will move with the quarry face until the final quarry depth is reached in each extraction area. At this there is sufficient separation from the quarry floor working areas. point, a permanent sump shall be established in each extraction area. During Phase 1, a new watercourse channel shall be constructed along the east side of Thorold Townline Road **Extraction Area** Phase 3B (within Phase 1B) for the eventual realignment of the existing watercourse. As resource extraction is completed in 1. Proceed with stripping of overburden/topsoil. Phase 1B, this area will be filled with clay overburden material from on-site to an elevation ranging between 173 o 178 masl. The new watercourse and riparian wetland channel shall be constructed, designed and vegetated in 2. Commence Phase 5 extraction in an easterly direction, moving gradually from north to south. accordance with DFO's authorization and this Rehabilitation Plan (drawing 5 of 6). 3. Phase 5 shall be extracted in up to three (3) lifts to a depth ranging between 140 masl and 143 masl. As extraction reaches the final quarry floor, and there is sufficient separation from the quarry floor working areas 4. Continue progressive rehabilitation of the quarry perimeter where limits of extraction have been reached and in Phase 1A, a 2:1 sideslope along the easterly and northerly limit of Phase 1B shall be backfilled with either: (i) there is sufficient separation from the quarry floor working areas. overburden stockpiled on-site; (ii) overburden in Phase 2; or (iii) material imported from Licence Numbers 11175 H. Final Phase 7. Commence site preparation of Phase 2. 1. Complete extraction of any remaining resource in the extraction limit near the entrance in Phase 1A and 1B (e.g. Stamford Lot 118 D. Phase 2 (2A & 2B) Stamford Lot 121 2. As part of the final operations of the site, remove office/scale house and scales, asphalt plant, recycled asphalt 1. Commence extraction in the 'Initial Sinking Cut Area' identified in the North Extraction Area (see plan view for material and any other equipment and scrap from the site. Stamford Lot 119 2. Phase 2A shall be extracted in up to three (3) lifts to a depth ranging between 141 masl to 145 masl. 3. Continue with final rehabilitation of the site. Complete quarry face backfilling on the remaining quarry faces as identified on drawing 5 of 6. 3. Phase 2B shall be extracted in one (1) to two (2) lifts to a depth of 155 masl. +++ 180.7 - Existing 145.5 - Max Depth Extraction Sequence Schematic Scale 1:7500 ++- 182.5 - Existing 145.0 - Max Depth Extraction Area 8m Acoustic Barrier (see note A.5 on drawing 4 of 6) - 100 Year Flood Line 100 Year Flood Line — Additional Lands Stage 2 Stage 1 Phase 1B Additional Lands Licensee transition area to be disturbed / extracted to a maximum depth of 175 masl to establish Stage 3 Stage 4 Phase 1B Phase 1B Undisturbed Site Preparation Under Extraction Progressive and Final Rehabilitation



# Site Plan Acronyms

- ARA Aggregate Resources Act
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- 7. ECA Environmental Compliance Approval
- 8. BMPP Best Management Practices Plan9. PTTW Permit to Take Water
- 10. MASL Metres above sea level
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- 12. ROW Right of way
- 13. HMA Hot mix asphalt14. PWQO Provincial Water Quality Objectives
- 15. MISA Municipal Industrial Strategy for Abatement
- 16. TSS Total Suspended Solids



walker

Walker Aggregates Inc. 2800 Thorold Townline Road P.O. Box 100 Thorold, Ontario L2V 3Y8

Upper's Quarry

Plan Scale: 1:3000 (Arch E)

Date

October 2021

Drawn By
C.P.

File No.

9811V

Eile Name

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Extraction Sequence 3 of 6

# A. Acoustic Assessment 1. Minimum 3 metre tall acoustic berms shall be constructed in the locations shown on the plan view. 2. The acoustic berms shall be constructed during site preparation and prior to extraction.

- 3. The primary crusher shall stay within 30 metres of the working face to maximize shielding effect of the quarry terrain,
- except when extraction is in the South Extraction Areas as per note A.4 below.
- 4. Material extracted from the South Extraction Area shall be processed in the Mid Extraction Area. . While processing in Phase 4, the licensee shall maintain an 8 metre tall barrier at a radius of 40 metres to the

southeast of the processing plant's secondary crushers (see plan view for location). The barrier can be material

- stockpiles, noise walls, or a combination of both. The barrier shall extend long enough to shield receptors R4 and R5 (see plan view) from the secondary crushers.
- 6. All construction equipment shall meet the sound emission standards defined in MECP Publication NPC-115. 7. The following best practice measures shall be undertaken to minimize the potential for construction noise impacts related to site preparation, berm creation and rehabilitation but not related to extraction and processing activities:
- a. Construction will be limited to time periods allowed by the City's applicable by-laws. If construction activities are required outside of these hours, the licensee will seek permits / exemptions directly from the City in advance.

b. All internal combustion engines will be fitted with appropriate muffler systems.

- c. The licensee's operating procedures will contain a provision that any initial complaint will trigger verification that the general noise control measures agreed to on this Plan are in effect.
- d. In the presence of persistent noise complaints, all construction equipment will be verified to comply with MECP's NPC-115 guidelines.
- e. In the event of verified noise complaints, alternative noise control measures may be required where reasonably available. In selecting appropriate noise control and mitigation measures, consideration will be given to the technical, administrative and economic feasibility of the various alternatives.

### B. Air Quality

- 1. The licensee shall apply water or another provincially approved dust suppressant to internal haul roads and processing areas, as necessary to mitigate dust.
- . Processing equipment shall be equipped with dust suppressing or collection devices, where the equipment creates dust and is operating within 300 metres of an air quality sensitive receptor (as set out in the Air Quality Impact
- 3. The licensee shall obtain an environmental compliance approval under the Environmental Protection Act where required to carry out operations at the quarry.
- . The site will operate in accordance with the Best Management Practices Plan (BMPP) for Fugitive Dust Emissions. The BMPP may be amended from time to time, considering actual impacts and operational considerations. The recommendations in the BMPP are based on the maximum daily production rates. At lower production rates, the

control measures specified in the BMPP can be reduced accordingly, provided dust remains mitigated on site.

- 5. The following mitigation measures shall be incorporated into the BMPP:
- a. Blasting operations occurring within 300 metres of a residential receptor shall have a smaller blast area, not exceeding 200 m<sup>2</sup> in area.
- b. Aggregate extraction, processing and shipping does not exceed 9,000 tonnes per day. c. Under dry conditions, the capacity to apply water on an hourly basis to all traveled haul routes within the licence

- 1. Areas identified as "Archaeological Site Protected Areas Requiring Further Archaeological Assessment" on this drawing reflect areas that require further archaeological assessment and are protected by a 20 to 30 metre protective buffer. A 50 metre monitoring buffer is also identified on this drawing.
- areas identified as "Archaeological Site Protected Areas Requiring Further Archaeological Assessment" and their respective protective buffers until: a. the required investigations are completed in accordance with the Stage 1 and 2 Archaeological Assessment

. No ground alterations including overburden stripping and excavation, or development of any kind shall occur within

prepared by Archaeological Research Associates Ltd. (April 2020), b. any recommendations that the respective site(s) has no further cultural heritage value or interest are made as a result of completing further investigations, and,

c. the associated reports are entered into the Ontario Public Register of Archaeological Reports and copies are

- 3. Until note C.2 has been satisfied, a A temporary barrier shall be established around the perimeter of each 'Archaeological Site - Protected Areas Requiring Further Archeological Assessment" identified on this drawing as part
- of site preparation and in advance of extraction ground alteration. 4. All soil disturbing activities within the 50 metres monitoring buffers shall be monitored by a licensed archaeologist to ensure the effectiveness of the avoidance strategy. The archaeologist shall ensure that the temporary barrier is in the appropriate location and shall be empowered to stop construction if there is a concern for impacts to an archaeological site. 'No go' instructions shall be issued to all work crews for the protected areas, and the locations of the protected areas shall be shown on all appropriate contract drawings. The protected areas shall be inspected by a licensed
- archaeologist once the strategy is no longer required, and the effectiveness of the strategy shall be reported to the F. Traffic Immediately upon issuance of the Licence, and once the construction schedule has been finalized, a licensed archaeologist will be retained by the licensee so that monitoring can occur where required. The remaining
- archaeological fieldwork will be completed upon issuance of the licence by the MND MNRF. 6. Should deeply buried archaeology remains be found during the course of site preparation and/or extraction related G. Visual activities, the MHSTCI shall be notified.
- 7. In the event that human remains are encountered during construction or extraction activities, the licensee shall immediately contact both the MHSTCl and Registrar or Deputy Registrar of the Cemeteries Regulation Unit of the Ministry of Government and Consumer Services (MGCS).

which supersedes this standard.

- 1. An attenuation study shall be undertaken by an independent blasting consultant during the first 12 months of operation in order to obtain sufficient quarry data to confirm the initial guideline parameters and assist in refining future blast
- 2. All blasts shall be monitored for both ground vibration and overpressure at the closest privately owned sensitive receptors adjacent the site, or closer, with a minimum of two (2) instruments - one installed in front of the blast and one
- Blasts shall be designed to maintain vibrations below 13mm/s at the location of the closest identified active spawning bed as per DFO guidelines. When blasting during active spawning season, a minimum of one supplemental vibration monitor shall be installed on the shoreline closest to the spawning bed to confirm the vibration levels.
- 4. The guideline limits for vibration and water overpressure shall adhere to standards as outlined in the Guidelines For the Use of Explosives In or Near Canadian Fisheries Waters (1998) or any such document, regulation or guideline
- All blasts shall be monitored for ground vibration at the adjacent Trans Canada Energy High Pressure Natural Gas Pipeline when blasting within 100m of the pipeline or when calculations suggest vibrations in excess of 35mm/s.
- . Blasts shall be designed to maintain vibrations at the transmission towers in the Hydro One Corridor below 50mm/s or any such document, regulation or corporate policy in effect at the time. When vibration calculations suggest vibrations
- at the towers may exceed 35mm/s, the towers shall be monitored for ground vibration. Blasts shall be designed to maintain vibrations at the 4832 Thorold Townline Road utility buildings below 50mm/s. When vibration calculations suggest vibrations at the utility buildings may exceed 35mm/s, the buildings shall be
- 3. The guideline limits for ground vibration and air overpressure shall adhere to standards as outlined in the Model Municipal Noise Control By-law publication NPC 119 (1978) or any such document, regulation or guideline which
- 9. Orientation of the aggregate extraction operation shall be designed and maintained so that the direction of the overpressure propagation will be away from structures as much as possible.
- 10. Blast designs shall be continually reviewed with respect to fragmentation, ground vibration and overpressure. Blast
- designs shall be modified as required to maintain compliance with current applicable guidelines and regulations. 11. Detailed blast records shall be maintained in accordance with current industry best practices.

# E. Natural Heritage

- a. Existing vegetation within the setbacks shall be maintained except where berms, haul roads and conveyors are
- b. New vegetation shall be maintained in accordance with note G.5 on this drawing
- c. Silt fencing shall be installed at the easterly limit of Phases 1A and 2A where field drainage enters the existing
- watercourse. Silt fencing will serve to demarcate the limit of protected area until the watercourse is diverted. d. Stockpiling of all excavated material shall be in accordance with note H.7 on drawing 2 of 6.
- e. Topsoil and overburden stockpiles shall be maintained in accordance with the Best Management Practices for the Protection, Creation and Maintenance of Bank Swallow Habitat in Ontario (MNRF 2017). Stripped overburden and topsoil for rehabilitation shall be utilized in accordance with notes E.4, E.5 and E.6 on drawing 2
- f. Dust control will be implemented in accordance with Section B on this drawing.
- g. Fuel storage shall be in accordance with the notes under Section K on drawing 2 of 6.
- 2. Natural Channel Design
- a. The existing watercourse will remain open (not culverted) where it enters the south limit of the South Extraction
- b. Where the watercourse exits the North Extraction Area, a culvert will be installed to maintain the watercourse while allowing an acoustic berm to be constructed. As part of final rehabilitation, the berm and culvert shall be removed to allow for the watercourse to be open.
- Area within Phase 2B, in accordance with the Natural Channel Design Report (Stantec 2021). The compensation pond will be excavated to a maximum depth of 174 masl in this area and in accordance with DFO authorization. No drilling or blasting shall occur in this Transition Area. d. As extraction is completed in Phases 1B and 2B, these areas will be filled with clay overburden material to an

c. As part of site preparation, a compensation pond will be constructed in the Watercourse Realignment Transition

- elevation ranging between 173 to 178 masl. In accordance with the Natural Channel Design Report (Stantec 2021), a new watercourse channel will be constructed, vegetated and designed in these areas and will include the following design elements:

d.1. Floodplain wetlands

- d.2. Fish habitat ponds, including new pike spawning habitat as well as foraging, spawning and rearing habitat for other fish species
- d.3. Creek sections d.4. Wood debris toe protection and wood reinforced banks
- d.5. Log sills d.6. Augmented riffle.
- e. Culverts will be installed under Upper's Lane and the unopened road allowance.
- f. 2:1 side slopes shall be established on the east side of the new watercourse channel down to the quarry floor.
- g. Once the realigned watercourse channel has been constructed in Phases 1B and 2B and adequate vegetation to mitigate potential erosion has been established (as confirmed by an ecologist), water from the existing watercourse will be diverted to the realigned watercourse in consultation with regulatory authorities. A fish rescue will be undertaken prior to dewatering and channel relocation. A License to Collect Fish for Scientific

# 3. Woodland and Terrestrial Habitat Enhancement

Purposes will be obtained for the fish rescue.

a. The 2.0 ha woodland situated on the east side of Thorold Townline Road shall be removed during the advancement of operations in Phase 1A/1B. Tree clearing in the woodlot shall be undertaken outside of the breeding bird period and the active bat season from March 23 and August 26.

- b. The lands identified off-site as "Woodland Compensation Area" on this drawing, an area of 4.7 ha, shall be planted in accordance with the Rehabilitation Plan (drawing 5 of 6).
- c. The lands identified on-site as Deciduous Woodland, Treed Deciduous Swamp and Swamp Thicket / Marsh
- Meadow on drawing 5 of 6, an area of 4.0 ha, shall be planted in accordance with the Rehabilitation Plan. d. Planting for the off-site woodland compensation will commence in the appropriate planting season following

# 4. Significant Wildlife Habitat and Wildlife

licence approval

- a. Vegetation clearing where milkweed plants are present will proceed when monarch larvae are absent (September 30 to April 1).
- b. The setbacks along Thorold Townline Road and Beechwood Road shall be planted with a mix of deciduous and coniferous trees and shrubs with a range of sizes. Native plant materials that are complementary to the regional and local landscape shall be used (see Rehabilitation Plan, drawing 5 of 6).

## Woodland and Wildlife Habitat Compensation Plan

- a. A woodland and wildlife habitat compensation plan shall be prepared in consultation with regulatory authorities to: (i) allow practices and management to respond to changing forest dynamics in the Woodland Compensation Areas such as pest infestations, climatic conditions (e.g. species selection) and restoration ecology; and (ii) achieve a net gain in the ecological functions of the local and regional landscape through:
- a.1. Increasing the total area of woodland cover in the regional landscape;

milkweed (Asclepias incarnata) and nectar producing plants.

- a.2. Improving associated landscape functions such as vegetative linkages and interior forest areas
- diversity, while retaining native genetics through seed collection and replanting. For example, prior to the removal of the existing 2 ha woodland:
- a.3.1. Tree seeds and nuts will be gathered from the woodland for direct planting in the Woodland Compensation Area to promote the continuity of local genetic stock and a similar community composition to the removed vegetation community (FOD9)

a.3. Improving forest ecological characteristics such as species diversity, age class distribution and structural

- a.3.2. Leaf litter and sods containing native understory vegetation will be transplanted to promote rapid establishment of a healthy forest soil microbiome
- a.3.3. Transplanting of native saplings and small shrubs from the woodland to the compensation planting area, where feasible.
- structures (bat boxes or condos), coniferous tree clusters for cover, browse-tolerant shrubs and mast producing trees; a.5. Incorporating specific planting in setbacks and the watercourse realignment channel. For example,

plantings that provide habitat for monarch including common milkweed (Asclepias syriaca), swamp

a.4. Incorporating specific wildlife habitat features for bats, deer and other wildlife, such as bat roosting

### 6. Fish and Fish Habitat

- a. Implement notes D.3 and D.4 on this drawing.
- b. Water shall be discharged from the sump area to the existing watercourse until water flow is diverted to the watercourse realignment channel. Once the watercourse realignment has been completed, water shall be discharged from the sump locations to the realigned watercourse. Pumping and discharge shall occur as required to support fish habitat.
- c. Water collected from the sump area shall be directed to a holding pond for storage to allow for settling of suspended solids and dissipation of other constituents such as hydrogen sulfide an alkalinity. Following this pond treatment, water will be discharged to the existing watercourse until water flow is diverted to the watercourse realignment channel. Once the watercourse realignment has been completed, water shall be discharged from the holding pond to the realigned watercourse. Pumping and discharge shall occur as required

to support fish habitat.

watercourse realignment channel.

- a. Wetlands along the existing watercourse will be maintained until the watercourse has been diverted to the
- b. Once the watercourse has been diverted, the created wetlands in the watercourse realignment channel shall be

mowing and maintenance.

American Elder

- a. A monitoring plan shall be prepared in consultation with regulatory authorities to assess the performance of the watercourse realignment channel and to confirm that impacts to off-site wetlands are not occurring as a result of
- b. A monitoring program of compensation planting shall be prepared in consultation with regulatory authorities to confirm stable conditions have been established.
- c. A trigger mechanism and contingency plan, as detailed in WSP's Water Study Report, shall be implemented upon licence approval to proactively ensure natural heritage features and their functions are maintained (i.e. fish habitat, wetland features downstream and at 5584 Beechwood Road, and woodlands) during operational and rehabilitation phases.
- 1. Prior to commencement of extraction operations, the required entrance improvements, road improvements and road widenings (to Thorold Townline Road) shall be completed to the satisfaction of the applicable road authorities and in general accordance with the figures titled "Uppers Lane Conceptual Intersection Design" and "Uppers Lane Vehicle
- 1. Where possible and to the extent to which it is present, existing vegetation located along the site perimeter within the
- setback area shall be retained. 2. 3.0 metre high acoustic berms and 2.4 metre high visual berms shall be established in the locations shown on the plan view. Berms shall be constructed in a smooth, rolling manner with varying highpoints (where space permits while respecting minimum height requirements), and variations along the berm frontage to create a more natural appearance. Berms shall be seeded with a naturalizing mix of wildflowers and grasses to stabilize slopes and minimize
- 3. Within the "Extended Planting Areas" (as shown on this drawing), trees shall be planted at a spacing of 5 to 10 metres on centre, depending on species. Where possible, plantings shall be randomly spaced and staggered up on the berm up to one third of its maximum height to appear more natural. Plantings shall also extend a minimum of 3 metres out from the berm towards the road where available space permits. All vegetation shall be selected for wind and salt tolerance and hardiness. Native non-invasive species that complement the existing surroundings shall be utilized.
- Where "Large Planting Stock" is indicated (see plan view and "Typical Visual Berm Detail" on this drawing), this area shall be planted with deciduous trees of minimum 40 millimetres caliper, coniferous trees of minimum 1.0 metre in height, and shrub species of minimum 40 centimetres height.

Where "Small Planting Stock" is indicated (see plan view and "Typical Visual Berm Detail" on this drawing), this area

- shall be planted with deciduous tree whips of minimum 1.2 metres in height, coniferous trees of minimum 0.6 metre in height, and shrub species of minimum 20 centimetres height (or bare root stock when in season). Planting shall occur for 40 metre stretches on either side of Upper's Lane and the unopened road allowance facing Thorold Town Line Road. The large planting stock shall be planted 3 metres beyond the berm and small planting stock
- shall extend from the toe of the berm to 2 metres up the berm. Plant species for berms may include, but shall not be limited to the following:

rees		
White Pine White Spruce Sugar / Silver Maple White Pine	Common Hackberry Paper Birch Trembling Aspen White Spruce	Chokecherry Pin Oak Basswood White Cedar
Shrubs		
Staghorn Sumac	Nannyberry	Common Nine

- 4. To ensure survival and positive growth rate, the vegetative screening shall be maintained as an effective visual screen
- over time. Allowance of natural succession is encouraged. 5. During the first year, planted trees shall be watered and monitored until established. After the first year and up to five years, trees shall be inspected biannually (end of Year 1, beginning of Year 3 and end of Year 4). Trees which are in

Highbush Cranberry

# 6. A mortality rate of up to 15% of all trees planted over the course of the five year maintenance period is expected. Trees that die exceeding this percentage shall be replaced yearly, preferably in the spring or late summer.

poor condition at the time shall be fertilized, watered and monitored to improve their health and vigor.

- A long-term monitoring program will be implemented during the quarry operational and rehabilitation phases, until stable conditions are observed after quarry decommissioning.
- . In the event a well interference claim is received, the licensee shall implement the following mitigation plan to protect the local groundwater users.
- a. Prior to extraction, landowners shall be provided with a copy of the water well interference plan as well as the contact information for the licensee and MECP (Wells Help Desk 1-888-396-9355 or email
- b. If a water well interference claim is received by the licensee the following actions shall be taken:
- b.1. The licensee shall immediately notify MNDMNRF and MECP of the complaint.
- b.2. The licensee shall contact a well contractor in the event of a well malfunction and residents will be provided a temporary water supply within 24 hours, if the issue cannot be easily determined and
- c. The well contractor shall contact the resident with the supply issue to rectify the problem as expediently as possible, provided landowner authorization of the work. d. If the issue raised by the landowner is related to loss of water supply, the licensee shall have a qualified hydrogeologist / well contractor determine the likely causes of the loss of water supply, which can result from a
- lack of well maintenance / well cleaning (owner's expense) or lowering of the water level in the well from the quarry development (licensee expense). This assessment process shall be carried out at the expense of the licensee and the results provided to the homeowner. e. If it has been determined that the quarry caused the water supply interference (i.e., lowering of the water level), the licensee shall continue to supply water at their expense until the problem is rectified. The following mitigation

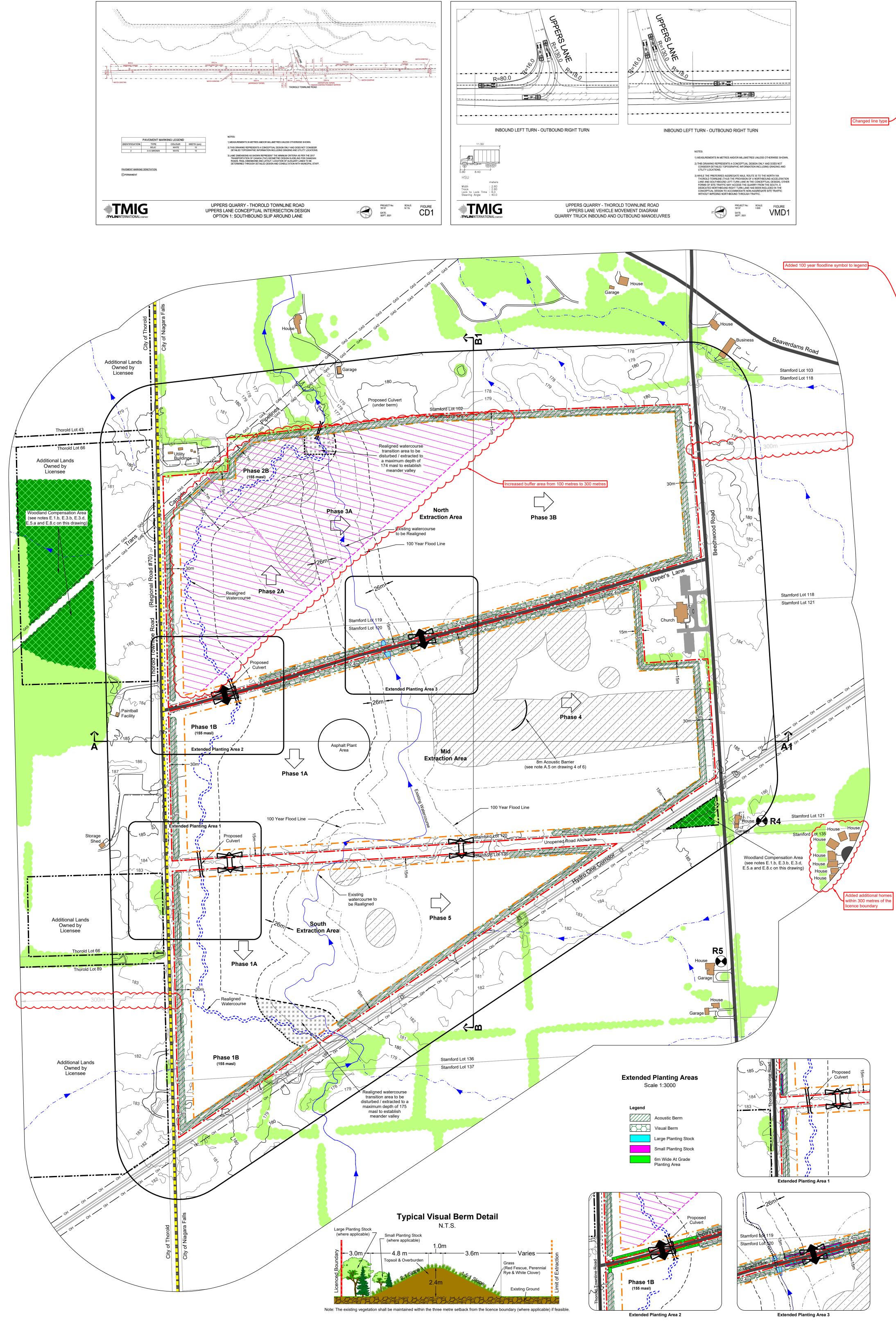
measures shall be considered, and the appropriate measure(s) implemented at the expense of the licensee:

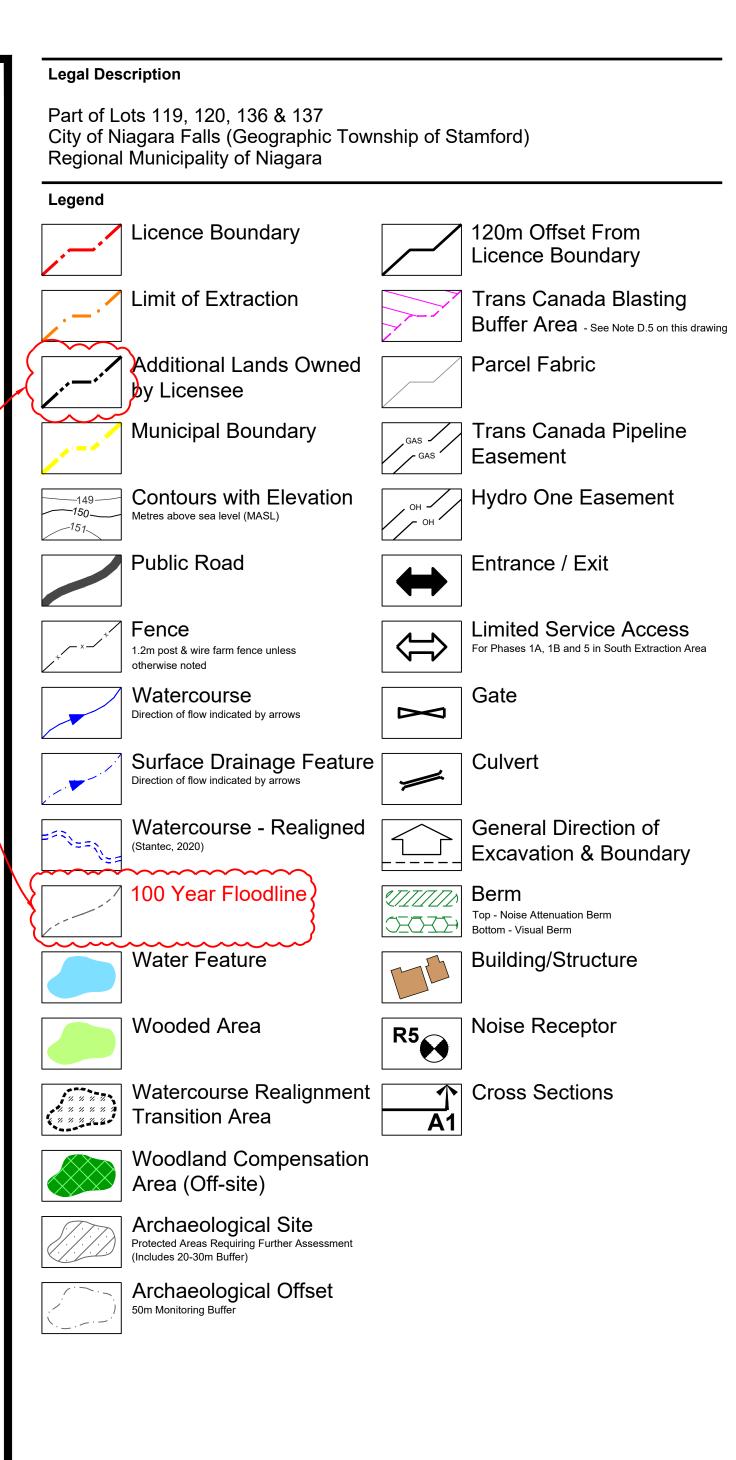
number of factors, including pump failure (owner's expense), extended overuse of the well (owner's expense),

- e.1. Adjust pump pressure;
- e.2. Lowering of the pump to take advantage of existing water storage within the well; e.3. Deepening of the well to increase the available drawdown, if the well deepening changes the water
- quality a water treatment shall be provided; e.4. Widening of the well to increase the available storage of water;

responsible for the expense to restore the water quality.

- e.5. Relocation of the well to another area on the property; or e.6. Drilling multiple wells.
- f. If the issue raised by the landowner is related to water quality, the licensee shall have a qualified hydrogeologist / well contractor determine the likely causes of the change in water quality, and review monitoring results at the quarry and background monitoring results from the baseline well survey to determine if there is any potential correlation with the quarry. If it has been determined that the quarry caused a water quality issue, the licensee shall continue to supply water at their expense until the problem is rectified. The licensee shall be responsible for restoring the water supply by replacing the well or providing a water treatment system. The licensee is
- A spill action plan shall be carried out in accordance with the notes in Section N Spills Plan on drawing 2 of 3.
- 4. A trigger mechanism and contingency plan as set out in WSP's Level 2 Water Study Report shall be implemented.
- 5. WSP's Water Study Report confirms that drawdown impacts do not extend to areas identified in the Niagara Peninsula Source Protection Plan as Intake Protection Zones.

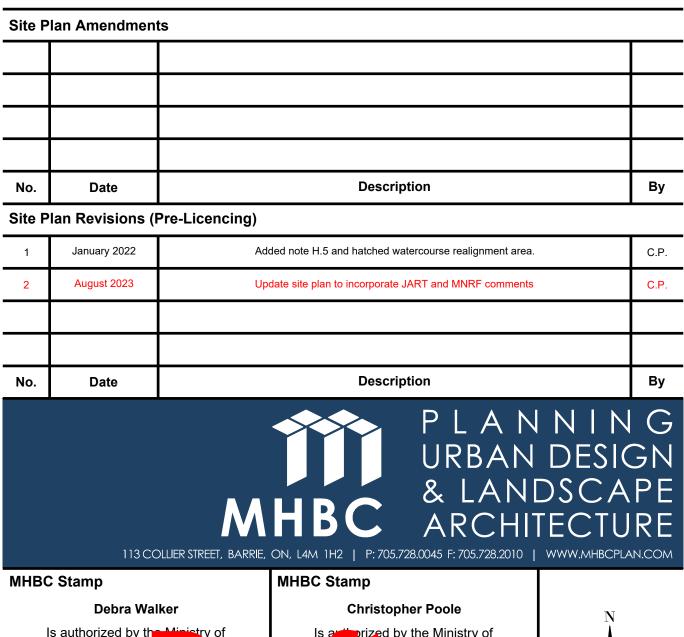




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- 12. ROW Right of way
- 13. HMA Hot mix asphalt 14. PWQO - Provincial Water Quality Objectives
- 15. MISA Municipal Industrial Strategy for Abatement

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prepare and certify site plans. prepare and certify site plans.

of Ontario Regulat

Walker Aggregates Inc. 2800 Thorold Townline Road P.O. Box 100 Thorold, Ontario L2V 3Y8

Subsection 0.2(3)(f)

gulation 244/97 to

Upper's Quarry

INDMNRF Licence Reference No. Applicant's Signature Plan Scale: 1:3000 (Arch E) October 2021

File Name **Report Recommendations** Drawing No.

4 of 6 File Path N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan.dwg

# PROGRESSIVE REHABILITATION

c.h. Undisturbed

d. To be rehabilitated outside of licence:

Table Report", dated October 2021.

A. General

Area calculations:			
a. Lice	enced area	103.6 I	
b. To l	pe extracted	89.1 h	
c. Fina	al rehabilitation within licence (total)	103.6 I	
c.a.	Lake	68.8 ha	
c.b.	Shoreline wetland	1.3 ha	
C.C.	Wetland/pond/stream	2.9 ha	
c.d.	Terrestrial	22.7 ha	
c.e.	Deciduous Woodland	1.2 ha	
c.f.	Treed Deciduous Swamp	2.0 ha	
c.g.	Swamp Thicket & Marsh Meadow	0.8 ha	

- d.a. Woodland Compensation Area 4.7 ha 2. The maximum predicted water table is 184.9 masl and the contact aquifer potentiometric contours ranges between 176.0 and 184.9 masl (as per WSP's "Proposed Upper's Quarry - Maximum Predicted Water
- B. Phasing
- 1. As excavation reaches the limit of extraction or maximum depth, progressive rehabilitation shall
- Progressive rehabilitation shall follow the general direction and sequence of extraction identified on the plan view and described in the notes on drawing 3 of 6. Minor deviations in operational/rehabilitation sequence will be permitted in order to adjust for any variable resource and market conditions. Any major deviations from the operations sequence shall require approval from the MNRF.
- 3. Prior to extraction commencing in Phases 3A and 3B, side sloping adjacent to Phases 1B and 2B shall be completed to allow for the existing watercourse realignment to be finalized.
- 4. Dewatering of the quarry will ultimately discharge to the watercourse (pre and post realignment). The quarry will continue dewatering operations to maintain a dry quarry floor. When the rock is fully extracted, it is proposed that dewatering operations will cease and the quarry will be permitted to fill naturally with surplus precipitation, surface water and any contribution from groundwater seepage to form a lake. As shown on the plan view, shallow shoreline wetland areas shall be created to provide aquatic habitat.
- Watercourse Realignment Channel Area As portions of the watercourse realignment channel are constructed, the channel shall be planted according to the requirements of each respective planting zone: (i) riparian planting zone; (ii) upland planting zone; (iii) shoreline planting zone and (iv) life staking planting zone. Details relating to construction, planting and monitoring requirements for the watercourse realignment corridor are contained within the "Natural Channel Design Report" prepared by Stantec Consulting Ltd. (dated October 2021).
- 6. Reforestation Areas There are two main reforestation areas:
- 6.1. The Woodland Compensation Area (Off-site) to be no less than 4.3 ha in area. Plantings in this area are set out in Table 1 on this drawing. Planting for this Area (Off-site) will commence in the appropriate planting season following licence approval.
- 6.2. The on-site Woodland Compensation Area includes the areas identified as the Deciduous Woodland, Treed Deciduous Swamp and Swamp Thicket/Marsh Meadow, to be no less than 4.0 ha in total area. Plantings in these areas are set out in Tables 1 to 3 on this drawing respectively. In the Deciduous Woodlands (on-site), additional conifer species will be added to the species mix to provide additional screening.
- 7. A woodland and wildlife habitat compensation plan shall be prepared in consultation with regulatory authorities in accordance with Note E.5.a on drawing 4 of 6.
- Slopes and Grading
- 1. Progressive rehabilitation will utilize a variety of rehabilitation techniques including:
  - a. backfilling extraction faces and quarry floors; or
- b. Leaving extraction faces vertical
- 2. Excess soil, as defined by Ontario Regulation 406/19 under the Environmental Protection Act, may be imported
- 2. Excess soil, as defined in Ontario Regulation 244/97 may be imported to this site to facilitate the following
- 2.1. To establish the final elevations, slopes and grades depicted on the plan view

2.2. Top dressing to establish vegetation

- 3. Liquid soil, as defined in Ontario Regulation 406/19 under the Environmental Protection Act, is not authorized for importation to the site.
- 4. The quality of excess soil imported to the site for final placement must be equivalent to or more stringent than the applicable excess soil quality standards as determined in accordance with Ontario Regulation 244/97, as amended from time to time, and must be consistent with the site conditions and the end use identified in the approved rehabilitation plan.
- 5. Where a qualified person is retained or required to be retained in accordance with Ontario Regulation 244/97, the quality, storage, and final placement of excess soils shall be done according to the advice of the qualified person.
- 6. Excess soil imported to facilitate rehabilitation as described on this site plan shall be undertaken in accordance with Ontario Regulation 244/97 under the Aggregate Resources Act, as amended from time
- 7. The cumulative total amount of excess soil that may be imported to this site for rehabilitation purposes is
- 3. Excess soil imported for the rehabilitation purposes described above shall meet the soil quality standards set out in Table 1: "Full Depth Background Site Condition Standards", of the Rules for Soil Management and Excess Soil Quality Standards published by the Ministry of Environment, Conservation and Parks, as amended from time to

# l. The maximum total amount of excess soil that may be imported to this site for rehabilitation purposes is

5. The licensee shall ensure that the acceptance and reuse of excess soil imported for rehabilitation purposes is compliant with Part 1: Rules for Soil Management of the "Rules for Soil Management and Excess Soil Quality

Standards published by the Ministry of Environment, Conservation and Parks, as amended from time to time.

- 8. The final rehabilitated landforms established using the rehabilitation techniques will consist of a lake, shoreline wetlands, riparian corridor, woodlands, gradually sloping grades, 2:1 and 3:1 side slopes, and vertical faces as shown on the plan view.
- D. Seeding and Planting
- 1. Side slopes steeper than 3:1 shall be seeded with a naturalizing mix of native, non-invasive wildflowers and grasses to stabilize slopes and minimize mowing and maintenance. the Ministry of Transportation's (MTO) Ontario Roadside Seed Mix (Creeping Red Fescue, Kentucky Bluegrass, Perennial Ryegrass and
- The deciduous woodlands, treed deciduous swamp, swamp thicket/marsh meadow, shoreline wetland, and realigned watercourse channel (riparian corridor) shall be planted with species identified in Tables 1-5 on this drawing respectively.

- 1. Final surface drainage will follow the rehabilitated contours and directional arrows shown on the plan
- 2. Once the quarry is depleted, pumping will cease and portions of the site below the ground water table will
- 3. The quarry dewatering discharge will be directed to the watercourse (pre and post alignment) and ultimately flow to Beaverdams Creek to support fish habitat and downstream wetlands.
- 4. The licensee shall operate in accordance with the conditions of the MECP, PTTW and ECA for the ongoing dewatering of the site.

# Trigger Mechanism and Contingency Plan

- 1. During progressive rehabilitation, until surrendering the licence, the licensee is required to operate in accordance with the Trigger Mechanism and Contingency Plan outlined below. included in the Upper's Quarry-Level 2 Water Study Report prepared by WSP, dated October 2021, as may be amended from time to time with approval from MNDMNRF.
- 2. The monitoring program will allow a comparison of observed conditions throughout the quarry development to baseline conditions. The predicted effects of the quarry have been reviewed and are based on the numerical groundwater model simulations and baseline water quality. Should the observed guarry effects differ from those predicted, a trigger mechanism has been developed to trigger the implementation of appropriate contingency measures to mitigate impacts before they occur. The guarry dewatering discharge will be directed to the Existing Watercourse, and ultimately flow to Beaverdams Creek. The discharge water will consist of a mixture of direct precipitation and groundwater inflows from the contact aguifer, shallow bedrock aguifer, deep bedrock aguifer and likely a small contribution from the underlying lower aquitard. The ratio of groundwater contribution from each unit is related to the relative hydraulic conductivities. Based on the hydraulic testing completed as part of this study, it is interpreted that the majority of the groundwater inflow will originate from the shallow bedrock aquifer. Therefore, it is predicted that the quarry discharge will have similar water quality to the shallow bedrock aquifer baseline ranges. The observed 2019 pumping test discharge water quality, which is predicted to be similar to the future quarry discharge water quality, supports this interpretation.
- 3. Monthly sampling of the quarry sump discharge has been included in the monitoring program, for the analysis of parameters with an associated Provincial Water Quality Objectives (PWQO), as well as selected parameters which aid in the assessment of influence from the various bedrock units. The trigger mechanism for the sump discharge to the Existing Watercourse is to assess the monthly sump water quality results against the list of trigger concentrations summarized in the table below.

Parameter	Proposed Trigger Mechanism	Applicable Standard
pH (pH units)	6.5 - 8.5	PWQO / MISA
TSS	25	MISA
Hydrogen Sulphide (undissociated)	0.002	PWQO
Total Oil and Grease	No visible sheen or odour	PWQO

- 4. The shallow bedrock aquifer groundwater is more mineralized / harder than the surface water in the vicinity of the Site; however, it satisfies the PWQO for most parameters. The two exceptions are undissociated hydrogen sulphide and total phosphorus. A trigger for hydrogen sulphide has been included in the trigger mechanism for quarry discharge. In the case of total phosphorus, the median total phosphorus concentration in the baseline surface water quality currently exceeds the PWQO, making the Existing Watercourse a Policy 2 receptor for this parameter. It is predicted that the total phosphorus concentration in the future quarry discharge will be below that of the upstream surface water in the Existing Watercourse. As such, total phosphorus has not been included in the trigger mechanism.
- 5. The Municipal Industrial Strategy for Abatement (MISA) was also considered; as such, pH, total suspended solids (TSS) and total oil and grease have also been included in the trigger mechanism.

- 6. The monthly sump discharge sample results shall be compared with the background conditions in the Existing Watercourse (station SW3) and Beaverdams Creek (station SW1). If parameter concentrations in the sump discharge exceed the above trigger concentrations without a corresponding exceedance in the background surface water, then weekly sampling of the quarry sump shall be initiated. Weekly sampling will continue until less than two parameter concentrations in the sump discharge exceed the trigger concentrations.
- 7. If weekly sampling is required for a period of more than four (4) weeks, contingency measures shall be implemented to reduce concentrations in the quarry discharge. Trigger exceedances for pH, TSS and total oil and grease would initiate a review of the design and operation of the quarry discharge sump. Where required, improvements shall be made to reduce discharge concentrations.
- 8. At existing pits and quarries within southern Ontario, hydrogen sulphide is typically not routinely included in the trigger mechanism. In southwestern Ontario, where the bedrock geology can favour hydrogen sulphide in groundwater, an Effluent Objective for hydrogen sulphide has been included in site ECAs. A sump or holding pond with a large surface area normally allows enough off-gassing of the hydrogen sulphide to meet the Effluent Objectives. For the quarry, the need for sufficient off-gassing of hydrogen sulphide shall be taken into consideration during the design and construction of the internal ditch network and sump pond for the Site. It is anticipated that the hydrogen sulphide concentration in the discharge to the Existing Watercourse will be lower than the PWQO / trigger concentration as a result of the off-gassing. If the hydrogen sulphide concentrations in the discharge are found to consistently exceed the trigger once the operational phase of the quarry begins, then a review of the design and operation of the internal ditch network and sump pond shall be completed with the objective of increasing the rate of off-gassing prior to discharge. Additional measures, such as aeration of the pond, may also be employed

### **FINAL REHABILITATION**

### G. General

1. All equipment and buildings/structures shall be removed from the licenced areas.

to enhance the off-gassing of hydrogen sulphide.

- 2. A fField/property access points entrance shall remain may be established to access the site for maintenance and monitoring purposes watercourse (as realigned). All operational access points shall be decommissioned and fenced as part of final rehabilitation.
- 3. The long term average surface water and lake level elevation is estimated to be approximately 175.15
- 4. At final rehabilitation, outflow from the realigned watercourse and the quarry lake will continue to discharge from the licence area at the present location where the existing watercourse channel crosses the northern licence boundary.

%	Botanical Name	Common Name	
TREES			Planting Notes:
5	Acer saccharum	Sugar Maple	Trees - woodland density 2,000/ha
25	Carya ovata	Shagbark Hickory	Shrubs - 3:1 Shrubs to trees - 6000/ha
15	Fagus grandifolia	American Beech	Ground Cover - application rate 22kg/ha
15	Ostrya virginiana	Ironwood	- cover crop of annual rye or oats 25kg/ha
20	Prunus serotina	Black Cherry	
5	Quercus rubra	Red Oak	
15	Tilia Americana	Basswood	
SHRUBS			
15	Amelanchier arborea	Juneberry	
20	Carpinus caroliniana	Blue-beech	
15	Hamamelis virginiana	Witch Hazel	
15	Prunus virginiana	Chokecherry	
20	Rhus typhina	Staghorn Sumac	
20	Cornus racemosa	Grey Dogwood	
15	Rubus odoratus	Purple-flowering Raspberry	
GROUND (	COVER	·	
20	Schizachyrium scoparium	Little Bluestem	
15	Elymus histrix	Bottlebrush grass	
15	Rudbeckia hirta	Black Eyed Susan	
15	Carex granularis	Meadow Sedge	
8	Solidago canadensis	Canada Goldenrod	
8	Oenothera biennis	Evening Primrose	
5	Asclepias syriaca	Common Milkweed	
5	Clematis virginiana	Virgin's Bower	
5	Monarda fistulosa	Wild Bergamot	
1	Anemone canadensis	Canada Anemone	
1	Euthamia graminifolia	Grass Leaved Goldenrod	
1	Symphyotrichum cordifolium	Heart-leaved Aster	
1	Aster novae-angliae	New England Aster	

## Table 2: Treed Deciduous Swamp Planting List

%	Botanical Name	Common Name		
TREES			Planting Notes:	
20	Acer x freemani	Freeman's Maple	Trees - Density treed deciduous swamp	
20	Juglans nigra	Black Walnut	1,200/ha	
20	Populus deltoides	Eastern Cottonwood	Shrubs - 3:1 Shrubs to trees - 3600/ha	
20	Quercus macrocarpa	Bur Oak	Ground Cover - application rate 22kg	
20	Thuja occidentalis Eastern White Cedar		- cover crop of annual rye or oats 25kg/h	
SHRUBS				
14	Cornus amomum	Silky Dogwood		
12	Cornus foemina	Gray Dogwood		
12	llex verticillata	Winterberry		
12	Rosa palustris	Swamp Rose		
12	Salix bebbiana	Bebb's Willow		
14	Spirea alba	Meadowsweet		
12	Viburnum lentago	Nannyberry		
12	Viburnum trilobum	American Cranberry-bush		

%	Botanical Name	Common Name	
HRUBS			Planting Notes:
14	Cornus amomum	Silky Dogwood	Shrubs - Thicket Shrubs- 3600/ha
12	Cornus foemina	Gray Dogwood	Ground Cover - application rate 22kg/ha
12	llex verticillata	Winterberry	- cover crop of annual rye or oats 25kg/ha
12	Rosa palustris	Swamp Rose	Live Stakes - 2 rows each with linea
12	Salix bebbiana	Bebb's Willow	spacing of 30 - 50 cm. offset ½ the linea spacing to stagger the stakes (Location
14	Spirea alba	Meadowsweet	and extent subject to on-site conditions a
12	Vibumum lentago	Nannyberry	the time of planting)
12	Vibumum trilobum	American Cranberry-bush	
IVE STA	KES		
34	Cornus sericea	Red Osier Dogwood	
33	Salix discolor	Pussy Willow	
33	Salix eriocephala	Heartleaf Willow	
VIARSH S	EED MIX		
20	Poa palustris	Fowl Bluegrass	
15	Carex vulpinoidea	Fox Sedge	
10	Verbena hastata	Blue Vervain	
10	Carex granularis	Meadow Sedge	
10	Euthamia graminifolia	Grass Leaved Goldenrod	
10	Asclepias incarnata	Swamp Milkweed	
5	Scirpus atrovirens	Dark Green Bulrush	
5	Juncus effusus	Soft Rush	
2	Eupatorium perfoliatus	Boneset	
2	Carex stipata	Stalk Grain Sedge	
2	Glyceria grandis	Tall Manna Grass	
2	Scirpus cyperinus	Woolgrass	
2	Eupatorium maculatum	Spotted Joe Pye Weed	
2	Carex bebbi	Bebb's Sedge	
1	Lobelia silphilitica	Blue Lobelia	
1	Symphyotrichum puniceum	Purple Stemmed Aster	

# Table 4: Shoreline Wetland

%	Botanical Name	Common Name
PLUGS		
10	Alisma plantago-aquatica	Water-plantain
15	Asclepias incarnata	Swamp Milkweed
10	Calla palustris	Wild Calla
10	Carex stricta	Tussock Sedge
10	Carex vulpinoidea	Fox Sedge
5	Chelone glabra	Turtlehead
5	Iris versicolor	Blue Flag Iris
10	Lemna minor	Little Duckweed
10	Polygonum amphibium	Water Smartweed
10	Sagittaria latifolia	Broad-leaved Arrowhead
5	Scirpus cyperinus	Wool-grass

Square Stemmed Monkey Flower

# Table 5: Riparian Planting List

1 Symphyotrichum puniceum

%	Common Name	Latin Name		
SHRUB	s			
14	Cornus amomum	Silky Dogwood		
12	Cornus foemina	Gray Dogwood		
12	llex verticillata	Winterberry		
12	Rosa palustris	Swamp Rose		
12	Salix bebbiana	Bebb's Willow		
14	Spirea alba	Meadowsweet		
12	Viburnum lentago	Nannyberry		
12 Viburnum trilobum		American Cranberry-bush		
LIKES	STAKES (Along Creek)	·		
34	Cornus sericea	Red Osier Dogwood		
33	Salix discolor	Pussy Willow		
33	Salix eriocephala	Heartleaf Willow		
RIPARI	AN SEED MIX			
20	Poa palustris	Fowl Bluegrass		
20	Carex granularis	Meadow Sedge		
10	Asclepias syriaca	Common Milkweed		
10	Verbena hastata	Blue Vervain		
10	Andropogon gerardii	Big Bluestem		
10	Juncus tenuis	Path Rush		
5	Rudbeckia hirta	Black Eyed Susan		
4	Solidago canadensis	Canada Goldenrod		
4	Clematis virginiana	Virgin's Bower		
4	Monarda fistulosa	Wild Bergamot		
1	Anemone canadensis	Canada Anemone		
1	Symphyotrichum novae-angliae	New England Aster		

Purple Stemmed Aster

Planting Notes: Shrubs - Riparian Shrubs- 3600/ha **Ground Cover** - application rate 22kg/ha - cover crop of annual rye or oats 25kg/ha. Live Stakes - 2 rows each with linear spacing of 30 - 50 cm. offset ½ the linear spacing to stagger the stakes (Location and extent subject to on-site conditions at the time of planting)

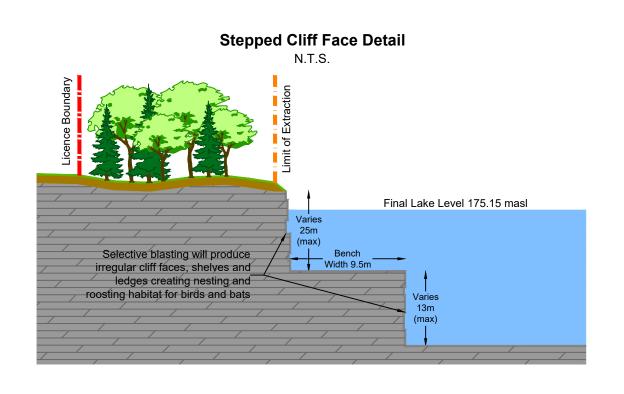
Plugs - 2 rows each with linear spacing of

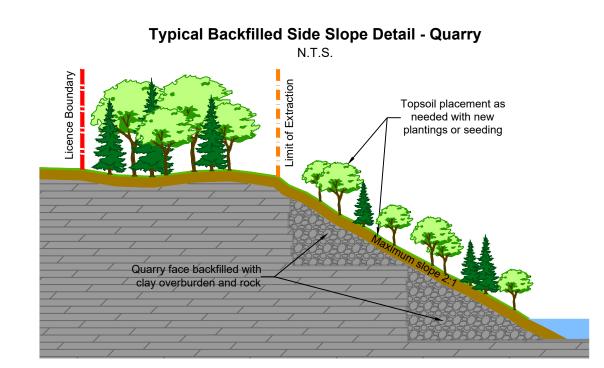
30 - 50 cm. offset ½ the linear spacing to

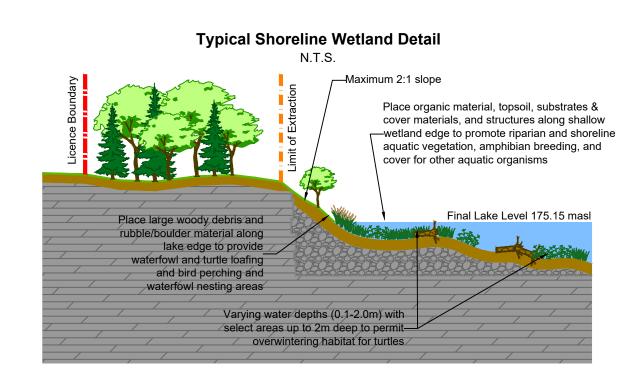
stagger the stakes (Location and extent

subject to on-site topographical conditions

at the time of planting)







Site Plan Acronyms

1. ARA - Aggregate Resources Act

2. MNDMNRF - Ministry of Northern Development, Mines, Natural Resources and Forestry

3. MHSTCI - Ministry of Heritage, Sport, Tourism and Culture Industries

4. MECP - Ministry of the Environment, Conservation and Parks

5. MGCS - Ministry of Government and Consumer Services

6. DFO - Department of Fisheries and Oceans Canada

7. ECA - Environmental Compliance Approval

8. BMPP - Best Management Practices Plan

14. PWQO - Provincial Water Quality Objectives

15. MISA - Municipal Industrial Strategy for Abatement

9. PTTW - Permit to Take Water

10. MASL - Metres above sea level

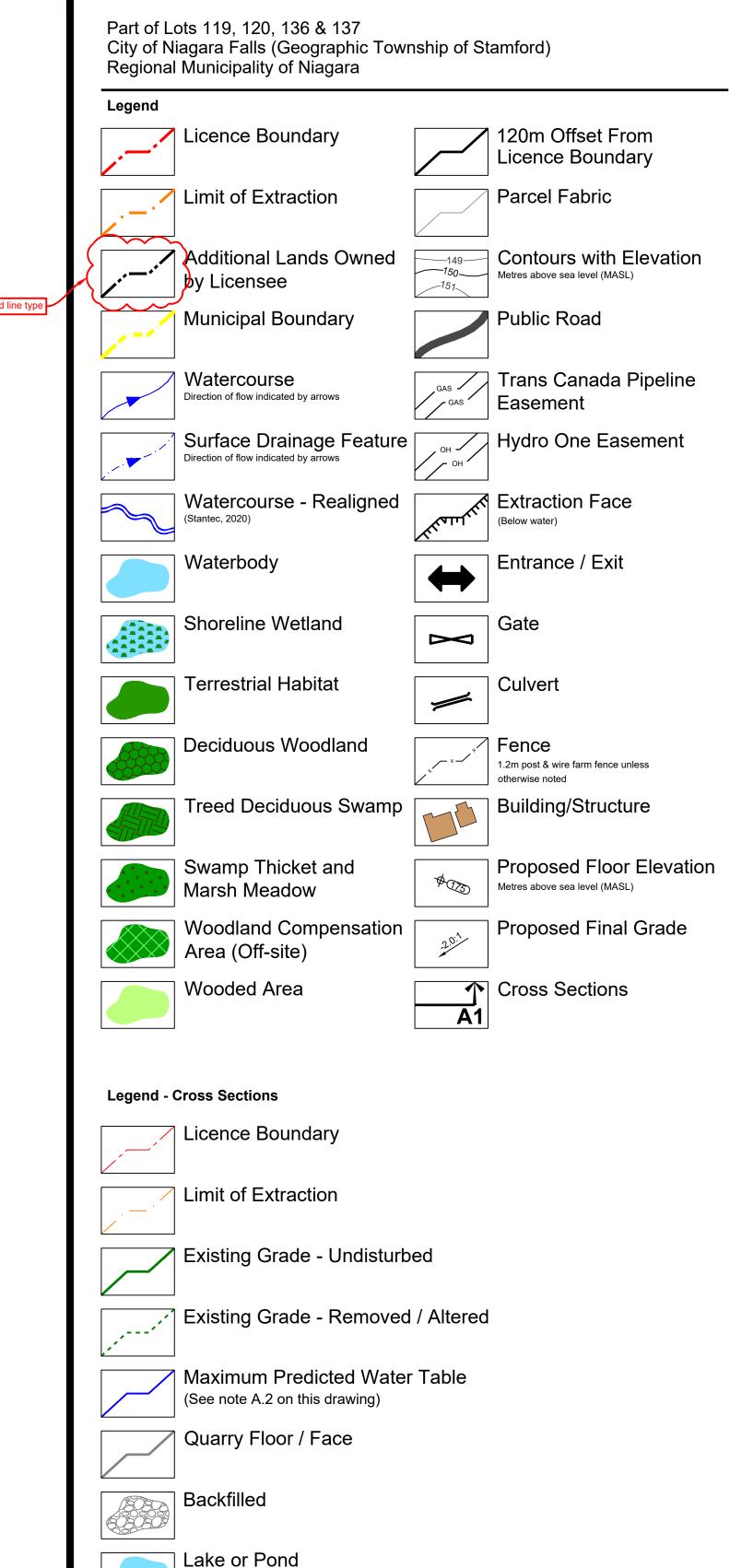
11. TCPL - Trans Canada Pipeline

16. TSS - Total Suspended Solids

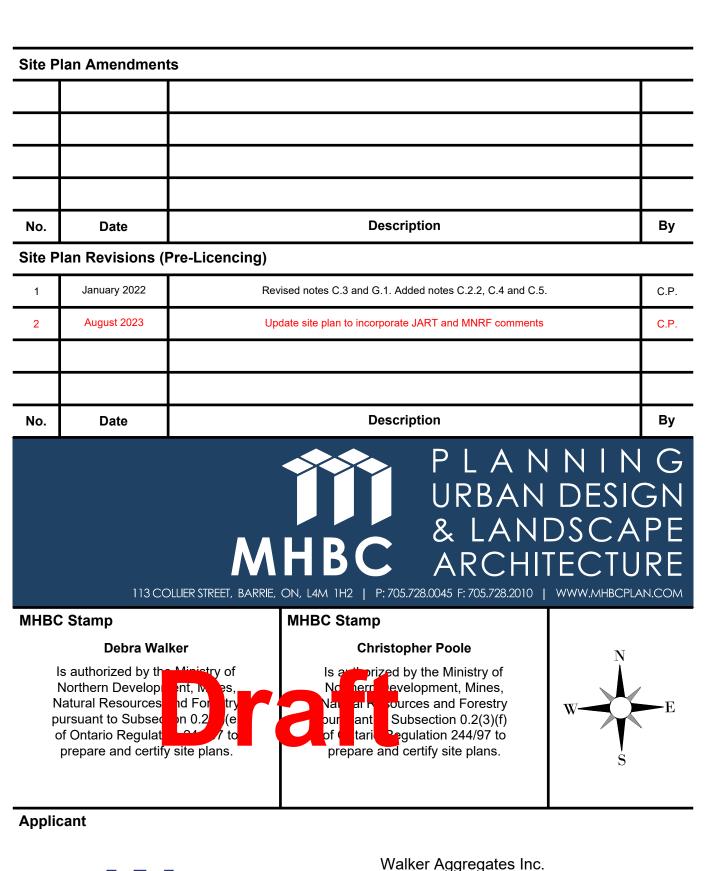
12. ROW - Right of way

13. HMA - Hot mix asphalt





**Legal Description** 





File Path

— → — Hydro Corridor

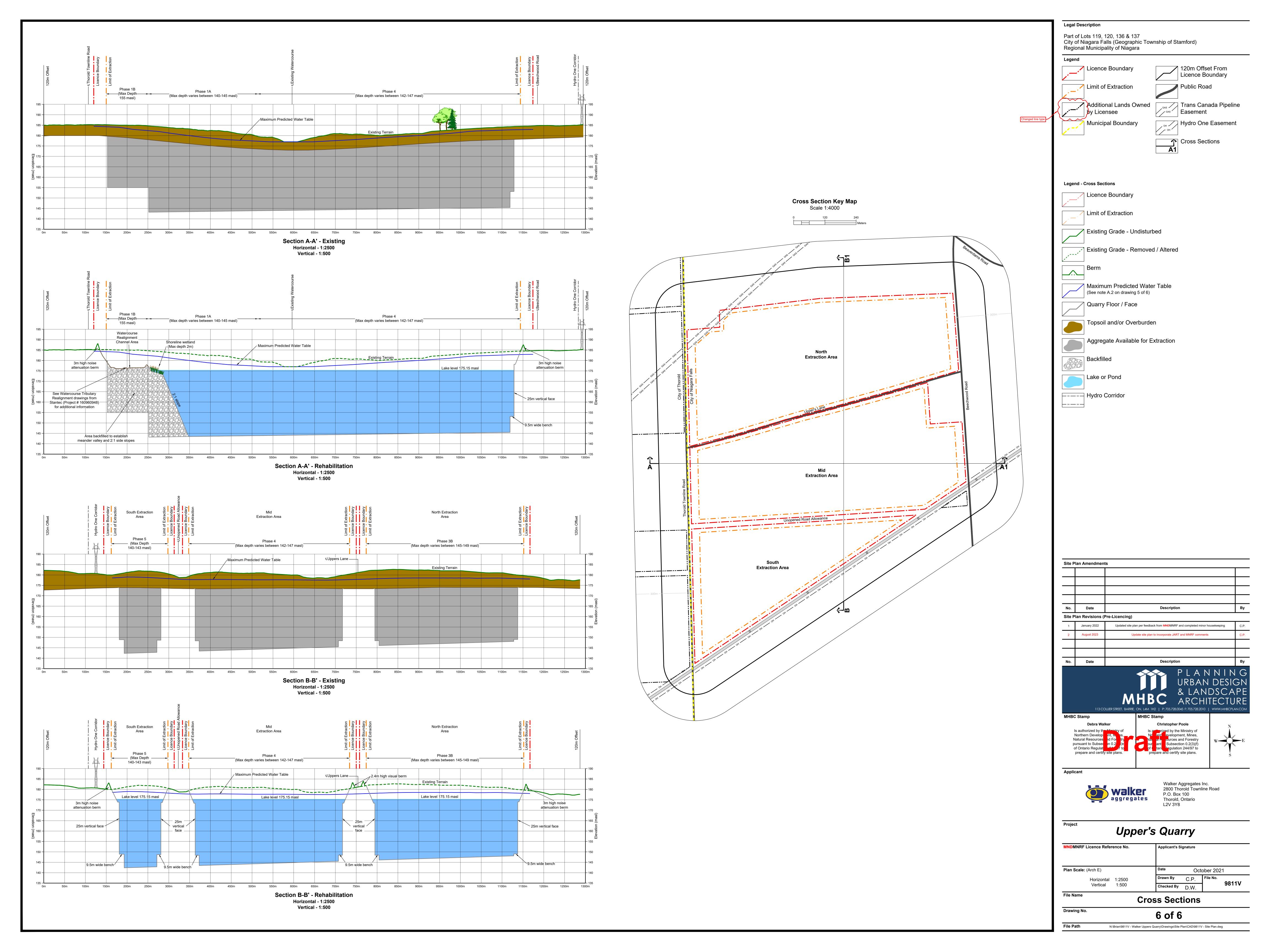
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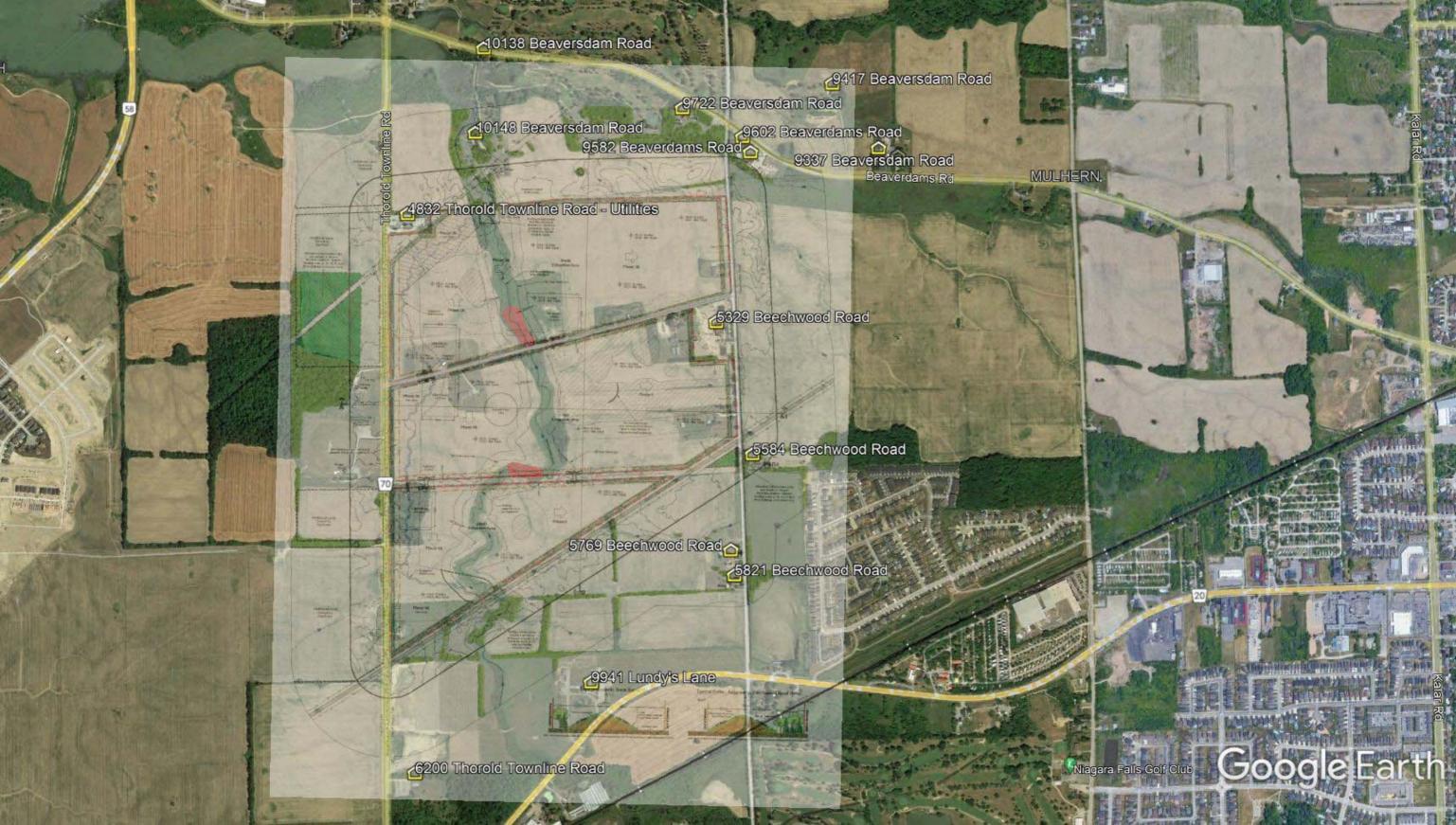
Walker Aggregates Inc. 2800 Thorold Townline Road P.O. Box 100 Thorold, Ontario L2V 3Y8

Upper's Quarry Applicant's Signature

**MND**MNRF Licence Reference No. Plan Scale: 1:3000 (Arch E) October 2021 File Name Rehabilitation Plan Drawing No. 5 of 6

N:\Brian\9811V - Walker Uppers Quarry\Drawings\Site Plan\CAD\9811V - Site Plan.dwg





# Appendix B



### **Uppers Quarry**

### PREVAILING METEOROLOGICAL CONDITIONS

Medians provided by Environment Canada Canadian Climate Normals 1981-2010 St Catherines – Municipal Airport

Date	Wind Direction	Max Hourly Wind Velocity Km/h	Temperature (Deg Celsius)
January	SW	89	-3.8
February	Е	63	-2.9
March	SW	74	1.1
April	SW	74	7.4
	OW	0.5	40.7
May	SW	65	13.7
June	SW	65	19.0
Juile	OVV	00	10.0
July	SW	63	21.9
August	W	59	20.8
September	W	53	16.6
October	SW	63	10.4
	011/		1.0
November	SW	70	4.6
D	CVA	70	0.0
December	SW	70	-0.9

# Appendix C

### **Ground Vibrations**

		<u> </u>							
<u>Imperia</u>	al Equations								
Equation 1		Equation 2		Equation 3		Equation 4		Equa	ition 5
Oriard 50% Bound (2002)		Oriard 90% Bound (2002)		Typical Production Blast (Bulletin 656 – 1971)		Typical limestone Quarry (Pader report – 1995)			Coal Mine 7 1980)
$v = 160 \left(\frac{D}{\sqrt{W}}\right)^{-1.6}$		v = 242(-	$v = 242(\frac{D}{\sqrt{W}})^{-1.6}$ $v = 182(\frac{D}{\sqrt{W}})^{-1.82}$		$v = 52.2(\frac{D}{\sqrt{W}})^{-1.38}$		v = 133(	$\frac{D}{\sqrt{W}}$ ) <sup>-1.5</sup>	
Metric Equations									
Equation 1		Equation 2		Equation 3		Equation 4			
DuPont General (1968)		Construction Blasting (Dowding 1998)		Agg. Quarry Blasting (Explotech 2005)		Agg. Quarry blasting (Explotech 2003)			
$v = 1140 \left(\frac{D}{\sqrt{W}}\right)^{-1.6}$		$v = 1326(\frac{D}{\sqrt{W}})^{-1.38}$		$v = 5175(\frac{D}{\sqrt{W}})^{-1.76}$		$v = 7025 (\frac{D}{\sqrt{W}})^{-1.85}$			
<u>-</u>							-		
D (m)	W (Kg)	PPV1 (mm/s)	PPV2 (mm/s)	PPV3 (mm/s)	PPV4 (mm/s)	PPV5 (mm/s)	PPV1 (mm/s)	PPV2 (mm/s)	PPV3 (mm/s)
710	118	1.4	2.2	0.5	1.4	1.9	1.4	4.1	3.3

### Air Overpressure

Imperial E	<u>equations</u>							_
Equat	tion 1	Equat	tion 2	E	quation 3	Equation 4		
USBM RI8485 (Behind Blast)		USBM RI8485 (Front of Blast)		USBM RI8485 (Full Confined)		Construction Average		
$P = 0.056 \left(\frac{D}{\sqrt[3]{W}}\right)^{-0.515}$		$P = 1.317 \ (\frac{D}{\sqrt[3]{W}})^{-0.966}$		$P = 0.061 \left(\frac{D}{\sqrt[3]{W}}\right)^{-0.96}$		$P = 1\left(\frac{D}{\sqrt[3]{W}}\right)^{-1.1}$		
Metric Equations								•
Equation 1		Equation 2		E	quation 3			
Ontario Quarry (Explotech 2013)		Limestone (Explotech 2011)		Ontario Quar	ry (Explotech 2012)			
$P = 159 \left(\frac{D}{\sqrt[3]{W}}\right)^{-0.0456}$		$P = 206 \left(\frac{D}{\sqrt[3]{W}}\right)^{-0.1}$		P=1222	$\left(\frac{D}{\sqrt[3]{W}}\right)^{-0.669}$			
D (m)	\\/ ( \/ er\)	OD4 (4D)	OD2 (AD)	OD3 (4D)	OD4 (dD)	OD4 (4D)	OD3 (4D)	
D (m)	W (Kg)	OP1 (dB)	OP2 (dB)	OP3 (dB)	OP4 (dB)	OP1 (dB)	OP2 (dB)	0
710	118	119.3	123.6	97.3	114.4	126.7	125.3	

# Appendix D



### Robert J. Cyr, P. Eng.

Principal, Explotech Engineering Ltd.

### **EDUCATION**

Bachelor of Applied Science, Civil Engineering, Queen's University

### PROFESSIONAL AFFILIATIONS

Association of Professional Engineers of Ontario (APEO)

Association of Professional Engineers and Geoscientists of BC (APEG)

Association of Professional Engineers, Geologists and Geophysicists of Alberta

Association of Professional Engineers and Geoscientists of New Brunswick

Association of Professional Engineers of Nova Scotia

Association of Professional Engineers and Geoscientists Manitoba

Professional Engineers and Geoscientists Newfoundland and Labrador

Northwest Territories and Nunavut Association of Professional Engineers (NAPEG)

International Society of Explosives Engineers (ISEE)

Ontario Stone Sand & Gravel Association (OSSGA)

Surface Blaster Ontario Licence 450109

### **SUMMARY OF EXPERIENCE**

Over thirty five years experience in many facets of the construction and mining industry has provided the expertise and experience required to efficiently and accurately address a comprehensive range of engineering and construction conditions. Sound technical training is reinforced by formidable practical experience providing the tools necessary for accurate, comprehensive analysis and application of feasible solutions. Recent focus on vibration analysis, blast monitoring, blast design, damage complaint investigation for explosives consumers and specialized consulting to various consulting engineering firms.

### PROFESSIONAL RECORD

2001 – Present	-Principal, Explotech Engineering Ltd.
1996 – 2001	-Leo Alarie & Sons Limited - Project Engineer/Manager
1993 – 1996	-Rideau Oxford Developments Inc. – Project Manager
1982 – 1993:	-Alphe Cyr Ltd. – Project Coordinator/Manager



### Mitch Malcomson, P.Eng.

Consulting Engineer, Explotech Engineering Ltd.

### **EDUCATION**

Bachelor of Engineering,
Civil Engineering with Concentration in Business Management,
Carleton University

### **PROFESSIONAL AFFILIATIONS**

Association of Professional Engineers of Ontario (APEO)
Association of Professional Engineers and Geoscientists of BC (APEG)
International Society of Explosives Engineers (ISEE)
Ontario Stone Sand and Gravel Association (OSSGA)

### **SUMMARY OF EXPERIENCE**

A Consulting Engineer and Project Manager for Explotech Engineering Ltd., Mitch holds a Bachelor of Engineering degree from Carleton University in Civil Engineering with a Concentration in Business Management. Mitch has strong analytical, technical, business and leadership skills. As a Project Manager, Mitch is responsible for operational strategies, scheduling and contract procurement. As a Consulting Engineer, the technical responsibilities include detailed blast designs, blast investigations and reviews, implementation of vibration monitoring programs, development of monitoring equipment/ technologies and building assessments for construction and the drilling and blasting portions of mining, quarrying and construction projects across Canada.

### PROFESSIONAL RECORD

2008 - Present - Consulting Engineer / Project Manager, Explotech Engineering Ltd.



### Andrew Campbell, P.Eng.

Explotech Engineering Ltd.

### **EDUCATION & QUALIFICATIONS**

Bachelor of Engineering, Mechanical Engineering, Carleton University

Advanced and Expert (Industry) CadnaA Modelling DataKustik, Mississauga, Ontario

### PROFESSIONAL AFFILIATIONS

Association of Professional Engineers of Ontario (APEO) International Society of Explosive Engineers (ISEE)

### SUMMARY OF EXPERIENCE

An engineer working for Explotech Engineering Ltd., Andrew holds a Bachelor of Engineering degree in Mechanical Engineering and has strong analytical, technical, and interpersonal skills. A proven leader in collaborative environments, Andrew is comfortable managing projects, specifying details, and communicating internally and externally. With a focus on blast designs, blast impact analyses, noise monitoring and modelling, damage complaint investigations, vibration analysis, and blast monitoring, Andrew has applied these skills across Canada.

### PROFESSIONAL RECORD

2018 – Present - Engineer, Explotech Engineering Ltd.

2013 – 2018 - Technician / EIT, Explotech Engineering Ltd.

2012 – 2012 - Ride Technician, Canada's Wonderland



### Michael Tobin, P.Eng.

Explotech Engineering Ltd.

### **EDUCATION**

Bachelor of Applied Science, Geological Engineering, Queen's University

### PROFESSIONAL AFFILIATIONS

Association of Professional Engineers of Ontario (APEO) International Society of Explosives Engineers (ISEE)

### **SUMMARY OF EXPERIENCE**

An engineer working for Explotech Engineering Ltd., Michael holds a Bachelor of Applied Science degree from Queen's University in Geological Engineering. Michael has strong analytical, technical, and interpersonal skills. Recent projects have focused on blast monitoring, vibration analysis, job estimation, damage complaint investigation and blast design.

### PROFESSIONAL RECORD

2021 – Present - Engineer, Explotech Engineering Ltd.

2017 – 2021 - Technician, Explotech Engineering Ltd.

1-866-EXPLOTECH

# Appendix E



### **Blasting Terminology**

ANFO: Ammonium Nitrate and Fuel Oil – explosive product

ANFO WR: Water resistant ANFO

Blast Pattern: Array of blast holes

Body hole: Those blast holes behind the first row of holes (Face Holes)

Burden: Distance between the blast hole and a free face

Column: That portion of the blast hole above the required grade

Column Load: The portion of the explosive loaded above grade

Collar: That portion of the blast hole above the explosive column,

filled with inert material, preferably clean crushed stone

Face Hole: The blast holes nearest the free face

Overpressure: A compressional wave in air caused by the direct action of

the unconfined explosive or the direct action of confining

material subjected to explosive loading.

Peak Particle Velocity: The rate of change of amplitude, usually measured in

mm/s or in/s. This is the velocity or excitation of the particles in the ground resulting from vibratory motion.

Scaled distance: An equation relating separation distance between a blast

and receptor to the energy (usually expressed as explosive

weight) released at any given instant in time.

Sensitive Receptor: Sensitive land use may include recreational uses which are

deemed by the municipality or provincial agency to be sensitive; and/or any building or associated amenity area (i.e. may be indoor or outdoor space) which is not directly associated with the industrial use, where humans or the

natural environment may be adversely affected by

emissions generated by the operation of a nearby industrial facility. For example, the building or amenity area may be associated with residences, senior citizen homes, schools,



day care facilities, hospitals, churches and other similar institutional uses, or campgrounds.

Spacing: Distance between blast holes

Stemming: Inert material, preferably clean crushed stone applied into

the blast hole from the surface of the rock to the surface of

the explosive in the blast hole.

Sub-grade: That portion of the blast hole drilled band loaded below the

required grade

Toe Load: The portion of explosive loaded below grade



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